

	□Submittal	☐ Substitution Request
Го:		
Firm:		
Project:		
Product Specified:		
Specified Location:		
		ect description, installation instructions and evaluation of the submittal request.
Submitted By:		
Name:	Si	ignature:
Firm:		
Address:		
		Fax:
Email:		Submittal Date:
For Architect / En	gineer Use:	
Reviewed, Accepte	d ~ No Exceptions:	Make Corrections as Noted:
Revise and Resubm	nit:	Rejected:
Brief explanation fo	or corrections needed	d, revisions needed or why rejected:

3.2.3.1	Product Description
3.2.3.2	Material Specifications
3.2.3.3	Strength Design
3.2.3.4	Technical Data
3.2.3.5	Installation Instructions
3.2.3.6	Ordering Information

Listings/Approvals

ICC-ES (International Code Council) ESR-3013

NSF/ANSI Std 61

certification for use in potable water COLA (City of Los Angeles)

RR 25881



Independent Code Evaluation

IBC°/IRC° 2009 (ICC-ES AC308)
IBC°/IRC° 2006 (ICC-ES AC308)
IBC°/IRC° 2003 (ICC-ES AC308)
IBC°/IRC° 2000 (ICC-ES AC308)
FBC° 2007

LEED®: Credit 4.1-Low Emitting Materials



The Leadership in Energy and Environmental Design (LEED®) Green Building Rating system™ is the nationally accepted benchmark for the design, construction and operation of high performance green buildings.

3.2.3.1 Product Description

Hilti HIT-HY 150 MAX-SD Adhesive Anchoring System is an injectable two-component hybrid adhesive. The two components are kept separate by means of a dual-cylinder foil pack attached to a manifold. The two components combine and react when dispensed through a static mixing nozzle attached to the manifold.

Hilti HIT-HY 150 MAX-SD Adhesive Anchoring System may be used with continuously threaded rod or deformed reinforcing bar installed in cracked or uncracked concrete. The primary components of the Hilti Adhesive Anchoring System are:

- Hilti HIT-HY 150 MAX-SD adhesive packaged in foil packs
- Adhesive mixing and dispensing equipment
- Equipment for hole cleaning and adhesive injection

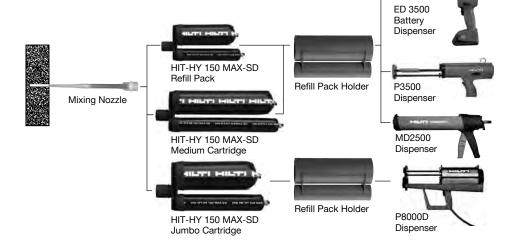
Product Features

- Superior bond performance in cracked and uncracked normal weight concrete
- Seismic qualified per IBC®/IRC® 2009, IBC®/IRC® 2006, IBC®/IRC® 2003 and IBC®/IRC® 2000 (ICC-ES AC308). Please refer to ESR-3013 (ICC-ES AC308) for Seismic Design Category A through F
- Mixing tube provides proper mixing, eliminates measuring errors and minimizes waste
- Contains no styrene; virtually odorless
- Excellent weathering resistance;
 Resistance against elevated temperatures

Fastener Components

HAS Threaded Rods

Rebar (supplied by contractor)



Guide Specifications

Master Format Section:

Previous 2004 Format

03250 03 16 00 (Concrete Anchors)

Related Sections:

03200 03 20 00 (Concrete Reinforcing) 05050 05 50 00 (Metal

Fabrications) **05120 05 10 00** (Structural Metal

Framing)

Injectable adhesive shall be used for installation of all reinforcing steel dowels or threaded anchor rods into new or existing concrete. Adhesive shall be furnished in side-by-side refill packs which keep component A and component B separate. Side-by-side packs shall be designed to compress during use to minimize waste volume. Side-by-side packs shall also be

designed to accept static mixing nozzle which thoroughly blends component A and component B and allows injection directly into drilled hole. Only injection tools and static mixing nozzles as recommended by manufacturer shall be used. Manufacturer's instructions shall be followed. Injection adhesive shall be formulated to include resin and hardener to provide optimal curing speed as well as high strength and stiffness. Typical curing time at 68°F (20°C) shall be approximately 30 minutes.

Injection adhesive shall be HIT-HY 150 MAX-SD, as furnished by Hilti.

Anchor Rods shall be furnished with chamfered ends so that either end will accept a nut and washer. Alternatively, anchor rods shall be furnished with a 45 degree chisel point on one end to allow for easy insertion into the adhesive-filled hole. Anchor rods shall be manufactured to meet the following requirements:

- 1. ISO 898 Class 5.8
- 2. ASTM A 193, Grade B7 (high strength carbon steel anchor);
- AISI 304 or AISI 316 stainless steel, meeting the requirements of ASTM F 593 (condition CW).

Special order length HAS Rods may vary from standard product.

Nuts and Washers of other grades and styles having specified proof load strength greater than the specified grade and style are also suitable. Nuts must have specified proof load strength equal to or greater than the minimum tensile strength of the specified threaded rod.

3.2.3.2 Material Specifications

Material Properties for Cured Adhesive

Compressive strength ¹	70	N/mm²	ISO 604
Compressive strength module (E-modulus) ¹	1350	N/mm²	ISO 604
Tensile strength @ break	9.5	N/mm²	ASTM D 638-97
Elongation @ break	2.75	%	ASTM D 638-97
Tensile modulus	2663	N/mm²	ASTM D 638
Flexural strength	42.83	N/mm²	ASTM D 790
Flexural modulus	2870	N/mm²	ASTM D 790
Volume shrinkage	3	%	ISO 3521
Linear shrinkage	3	%	
Water absorption (28 d)	5.3	%	ISO 62
pH value cured mortar	6		EN 1245
Thermal expansion coefficient	31	ppm/°C	
Specific contact resistance	2.17 x 10°	Ωxcm	DIN IEC 93
Specific surface resistance	5.05 x 10°	Ωxcm	DIN IEC 93
Electric strength	2.85	kV/mm	DIN VDE 303
UV stability cured mortar	Stable		EN ISO 4862-2

¹ Minimum values obtained as a result of three cure temperatures (23°, 40°, 60°F)

3.2.3.3 Strength Design^{1,2}

3.2.3.3.1 General: Design strengths are determined in accordance with ACI 318-08 Appendix D (ACI 318) and supplemented by ICC-ES ESR-3013.

Design parameters are provided in Table 5 through Table 19. Strength reduction factors, Φ , as given in ACI 318 D.4.4 must be used for load combinations calculated in accordance with Section 1605.2.1 of the IBC and Section 9.2 of ACI 318. Strength reduction factors, Φ , as given in ACI 318 D.4.5 must be used for load combinations calculated in accordance with ACI 318 Appendix C.

The following amendments to ACI 318 Appendix D must be used as required for the strength design of adhesive anchors. In conformance with ACI 318, all equations are expressed in inch-pound units.

Modify ACI 318 D.4.1.2 as follows:

D.4.1.2 — In Eq. (D-1) and (D-2), ΦN_a and ΦV_a are the lowest design strengths determined from all appropriate failure modes. ΦN is the lowest design strength in tension of an anchor or group of anchors as determined from consideration of ΦN_{sa} , either ΦN_{a} or ΦN_{aq} and either ΦN_{cb} or ΦN_{cbq} . ΦV_n is the lowest design strength in shear of an anchor or a group of anchors as determined from consideration of: ΦV₂₂, either $\Phi V_{_{\text{cb}}}$ or $\Phi V_{_{\text{cbg}}}$, and either $\Phi V_{_{\text{cp}}}$ or ΦV_{cpq}. For adhesive anchors subjected to tension resulting from sustained loading, refer to D.4.1.4 for additional requirements.

Add ACI 318 Section D.4.1.4 as follows:

D.4.1.4 — For adhesive anchors subjected to tension resulting from sustained loading, a supplementary check shall be performed using Eq. (D-1), whereby N_{ua} is determined from the sustained load alone, e.g., the dead load

and that portion of the live load acting that may be considered as sustained and ΦN_{\perp} is determined as follows:

D.4.1.4.1 — For single anchors, $\Phi N_n = 0.75 \Phi N_{a0}$.

D.4.1.4.2 — For anchor groups, Eq. (D-1) shall be satisfied by taking $\Phi N_n = 0.75 f N_{a0}$ for that anchor in an anchor group that resists the highest tension load.

D.4.1.4.3 — Where shear loads act concurrently with the sustained tension load, the interaction of tension and shear shall be analyzed in accordance with D.4.1.3.

Modify ACI 318 D.4.2.2 in accordance with 2009 IBC Section 1908.1.10 as follows:

D.4.2.2 — The concrete breakout strength requirements for anchors in tension shall be considered satisfied by the design procedure of D.5.2 provided Equation D-8 is not used for anchor embedments exceeding 25 inches. The concrete breakout strength requirements for anchors in shear with diameters not exceeding 2 inches shall be considered satisfied by the design procedure of D.6.2. For anchors in shear with diameters exceeding 2 inches, shear anchor reinforcement shall be provided in accordance with the procedures of D.6.2.9.

3.2.3.3.2. Static Steel Strength in

Tension: The nominal static steel strength of a single anchor in tension, N_{sa} , in accordance with ACI 318 D.5.1.2 and strength reduction factor, Φ , in accordance with ACI D.4.4 are given in the tables outlined in Table 1a for the corresponding anchor steel.

3.2.3.3.3. Static Concrete Breakout Strength in Tension: The nominal static

concrete breakout strength of a single anchor or group of anchors in tension, N_{cb} or N_{cbg} , must be calculated in accordance with ACI 318 D.5.2 with the following addition:

D.5.2.10 (2009 IBC) or D.5.2.9 (2006 IBC) — The limiting concrete strength of adhesive anchors in tension shall be calculated in accordance with D.5.2.1 to D.5.2.9 under the 2009 IBC or D.5.2.1 to D.5.2.8 under the 2006 IBC where the value of $k_{\rm c}$ to be used in Eq. (D-7) shall be:

 $k_{c,cr}$ where analysis indicates cracking at service load levels in the anchor vicinity (cracked concrete). The values of $k_{c,cr}$ are given in Tables 6, 9, 12, 15 and 18 of this document.

k_{c,uncr} where analysis indicates no cracking at service load levels in the anchor vicinity (uncracked concrete). The values of k_{c,uncr} are given in Tables 6, 9, 12, 15 and 18 of this document.

The basic concrete breakout strength of a single anchor in tension, $N_{\rm b}$, must be calculated in accordance with ACI D.5.2.2 using values of $h_{\rm ef}$, $k_{\rm c,cr}$ and $k_{\rm c,uncr}$ as decribed in the tables of this document. The modification factor " λ " shall be taken as 1.0. Anchors shall not be installed in lightweight concrete. The value of $f'_{\rm c}$ used for calculation must be limited to 8,000 psi (55 MPa) in accordance with ACI 318 D.3.5.

- 1 ACI 318-05 or 318-02 may also be used. The section references and terminology are different from those given in this section.
- 2 This section 3.2.3.3 is a reproduction of the content of ICC-SR 3013, representing the opinions and recommendations of ICC-SS.

3.2.3.3.4. Static Pullout Strength

in Tension: In lieu of determining the nominal static pullout strength in accordance with ACI 318 D.5.3, nominal bond strength in tension must be calculated in accordance with the following sections added to ACI 318:

D.5.3.7 — The nominal bond strength of a single adhesive anchor N_a , or group of adhesive anchors, N_{ag} , in tension shall not exceed

(a) for a single anchor

$$N_{a} = \frac{A_{Na}}{A_{Na0}} \cdot \psi_{ed,Na} \cdot \psi_{p,Na} \cdot N_{a0} \qquad (D-16a)$$

(b) for a group of anchors

$$N_{\text{ag}} = \frac{A_{\text{Na}}}{A_{\text{Na0}}} \cdot \psi_{\text{ed,Na}} \cdot \psi_{\text{g,Na}} \cdot \psi_{\text{ec,Na}} \cdot \psi_{\text{p,Na}} \cdot N_{\text{a0}} \tag{D-16b}$$

where:

 A_{Na} is the projected area of the failure surface for the single anchor or group of anchors that shall be approximated as the base of the rectilinear geometrical figure that results from projecting the failure surface outward a distance, $c_{cr,Na}$, from the centerline of the anchor, or in the case of a group of anchors, from a line through a row of adjacent anchors. A_{Na} shall not exceed nA_{Na0} where n is the number of anchors in tension in the group. In ACI 318 Figures RD.5.2.1a and RD.5.2.1b, the terms $1.5h_{ef}$ and $3.0h_{ef}$ shall be replaced with $c_{cr,Na}$ and $s_{cr,Na}$, respectively.

A_{Na0} is the projected area of the failure surface of a single anchor without the influence of proximate edges in accordance with Eq. (D-16c):

$$A_{Na0} = (s_{cr,Na})^2$$
 (D-16c)

with

 $s_{cr,Na}$ = as given by Eq. (D-16d).

D.5.3.8 — The critical spacing $s_{\rm cr,Na}$ and critical edge distance $c_{\rm cr,Na}$ shall be calculated as follows:

$$s_{cr,Na} = 20 \cdot d \sqrt{\frac{t_{k,uncr}}{1,450}} \le 3 \cdot h_{ef}$$
 (D-16d)
 $c_{cr,Na} = \frac{s_{cr,Na}}{2}$ (D-16e)

D.5.3.9 — The basic strength of a single adhesive anchor in tension in cracked concrete shall not exceed:

$$N_{a0} = \tau_{k,cr} \cdot \pi \cdot d \cdot h_{ef}$$
 (D-16f)

where:

 $\tau_{\text{k,cr}}$ is the bond strength in cracked concrete

D.5.3.10 — The modification factor for the influence of the failure surface of a group of adhesive anchors is:

$$\psi_{g,Na} = \psi_{g,Na0} + \left[\left(\frac{s}{s_{cr,Na}} \right)^{0.5} \cdot (1 - \psi_{g,Na0}) \right] (D-16g)$$

Where

$$\psi_{g,Na0} = \sqrt{n} - \left[(\sqrt{n} - 1) \cdot \left(\frac{\tau_{k,cr}}{\tau_{k,max,cr}} \right)^{1.5} \right] \ge 1.0$$
(D16h)

Where

n = the number of tension-loaded adhesive anchors in a group.

$$\tau_{k,\text{max,cr}} = \frac{k_{c,\text{cr}}}{\pi \cdot d} \cdot \sqrt{h_{\text{ef}} \times f'_{c}}$$
 (D-16i)

The value of f'_{c} must be limited to a maximum of 8,000 psi (55 MPa) in accordance with ACI 318 D.3.5.

D.5.3.11 — The modification factor for eccentrically loaded adhesive anchor groups is:

$$\psi_{\text{ec,Na}} = \frac{1}{1 + \frac{2e'_n}{s_{\text{cr,Na}}}} \le 1.0$$
 (D-16j)

Eq. (D-16j) is valid for
$$e_N^1 \le \frac{s}{2}$$

If the loading on an anchor group is such that only certain anchors are in tension, only those anchors that are in tension shall be considered when determining the eccentricity e'_N for use in Eq. (D-16j).

In the case where eccentric loading exists about two orthogonal axes, the modification factor $\psi_{\text{ec,Na}}$ shall be computed for each axis individually and the product of these factors used as $\psi_{\text{ec,Na}}$ in Eq. (D-16b).

D.5.3.12 — The modification factor for the edge effects for a single adhesive anchor or anchor groups loaded in tension is:

$$\psi_{\text{ed,Na}} = 1.0 \text{ when } c_{\text{a,min}} \ge c_{\text{cr,Na}}$$
 (D-16I)

$$\psi_{\text{ed,Na}} = \left(0.7 + 0.3 \cdot \frac{c_{\text{a,min}}}{c_{\text{cr,Na}}}\right) \le 1.0 \text{ when } c_{\text{a,min}} < c_{\text{cr,Na}}$$
(D-16m)

D.5.3.13 — When an adhesive anchor or a group of adhesive anchors is located in a region of a concrete member where analysis indicates no cracking at service load levels, the nominal strength, N or N_{aq}, of a single adhesive anchor or a group of adhesive anchors shall be calculated according to Eq. (D-16a) and Eq. (D-16b) with $\tau_{k.uncr}$ substituted for $\tau_{k.cr}$ in the calculation of the basic strength N₂₀ in accordance with Eq. (D-16f). The factor $\psi_{q,Na0}$ shall be calculated in accordance with Eq. (D-16h) whereby the value of $\psi_{k \max uncr}$ shall be calculated in accordance with Eq. (D-16n) and substituted for $\tau_{k,max,cr}$ in Eq. (D-16h).

$$\tau_{k,\text{max,uncr}} = \frac{\tau_{k,\text{uncr}}}{\pi \cdot d} \cdot \sqrt{h_{\text{ef}} \cdot f_{\text{c}}'} \qquad \text{(D-16n)}$$

D.5.3.14—When an adhesive anchor or a group of adhesive anchors is located in a region of a concrete member where analysis indicates no cracking at service load levels, the modification factor $\psi_{p,Na}$ shall be taken as:

$$\psi_{p,Na}$$
 = 1.0 when $c_{a,min} \ge c_{ac}$ (D-16o)

$$\psi_{\text{p,Na}} = \frac{\text{max} \mid c_{\text{a,min}}; c_{\text{cr,Na}} \mid}{c_{\text{ac}}} \text{ when } c_{\text{a,min}} \leq c_{\text{ac}}$$
 (D-16p)

where:

 $c_{\mbox{\tiny ac}}$ shall be determined in accordance with Section 3.2.3.3.10 of this document.

For all other cases: $c_{p,Na} = 1.0$ (e.g. when cracked concrete is considered).

Additional information for the determination of nominal bond strength in tension is given in Section 3.2.3.3.8 of this document.

3.2.3.3.5. Static Steel Strength in

Shear: The nominal static steel strength of a single anchor in shear as governed by the steel, V_{sa} , in accordance with ACI 318 D.6.1.2 and strength reduction factor, Φ , in accordance with ACI 318 D.4.4 are given in the tables outlined in Table 1a of this document for the corresponding anchor steel.

3.2.3.3.6. Static Concrete Breakout Strength in Shear: The nominal static concrete breakout strength of a single anchor or group of anchors in shear, V_{ch} or V_{cba}, must be calculated in accordance with ACI 318 D.6.2 based on information given in the tables outlined in Table 1a of this document for the corresponding anchor steel. The basic concrete breakout strength of a single anchor in shear, V, must be calculated in accordance with ACI 318 D.6.2.2 using the values of d given in the tables outlined in Table 1a for the corresponding anchor steel in lieu of d (IBC 2009) and d_o (IBC 2006). In addition, $h_{_{ef}}$ must be substituted for $\ell_{_{e}}$. In no case shall h_{ef} exceed 8d. The value of f'_{ef} must be limited to a maximum of 8,000 psi (55 MPa) in accordance with ACI 318 D.3.5.

3.2.3.3.7. Static Concrete Pryout Strength in Shear: In lieu of determining the nominal static pryout strength in accordance with ACI 318 D.6.3.1, the nominal pryout strength in shear must be calculated in accordance with the following sections added to ACI 318:

D.6.3.2 — The nominal pryout strength of an adhesive anchor or group of adhesive anchors shall not exceed:

(a) for a single adhesive anchor:

$$V_{cp} = min | k_{cp} \cdot N_a; k_{cp} \cdot N_{cb} |$$
 (D-30a)

(b) for a group adhesive anchors:

$$V_{cpg} = min | k_{cp} \cdot N_{ag}; k_{cp} \cdot N_{cbg} |$$
 (D-30b) where:

 k_{cp} = 1.0 for h_{ef} < 2.5 inches (64 mm)

 $k_{cp} = 2.0$ for $h_{ef} \ge 2.5$ inches (64 mm)

 N_a shall be calculated in accordance with Eq. (D-16a).

 N_{ag} shall be calculated in accordance with Eq. (D-16b).

 N_{cb} and N_{cbg} shall be determined in accordance with D.5.2.

3.2.3.3.8. Bond Strength

Determination: Bond strength values are a function of the concrete compressive strength, whether the concrete is cracked or uncracked and the installation conditions (dry, water-saturated concrete). The resulting characteristic bond strength must be multiplied by the associated strength reduction factor Φ_{nn} as follows:

Concrete Type	Permissible Installation Conditions	Bond Strength	Associated Strength Reduction Factor		
ıcked	Dry	$ au_{ ext{k,uncr}}$	Φ_{d}		
Uncracked	Water- saturated	$ au_{ ext{k,uncr}}$	Φ _{ws}		
ked	Dry	$ au_{k,cr}$	Φ _d		
Cracked	Water- saturated	$ au_{k,cr}$	Φ _{ws}		

Figure 2 of this document presents a bond strength design selection flowchart. Strength reduction factors for determination of the bond strength are given in the tables outlined in Table 1a of this document. Adjustments to the bond strength may also be taken for increased concrete compressive strength. These factors are given in the corresponding tables as well.

3.2.3.3.9. Minimum Member Thickness,

 \mathbf{h}_{min} , Anchor spacing, \mathbf{s}_{min} , and Edge Distance, \mathbf{c}_{min} : In lieu of ACI 318 D.8.3, values of \mathbf{c}_{min} and \mathbf{s}_{min} described in this document must be observed for anchor design and installation. In lieu of ACI 318 D.8.5, the minimum member thicknesses, \mathbf{h}_{min} , described in this document must be observed for anchor design and installation. In determining minimum edge distance, \mathbf{c}_{min} , the following section must be added to ACI 318:

D.8.8 — For adhesive anchors that will remain untorqued, the minimum edge distance shall be based on minimum cover requirements for reinforcement in 7.7. For adhesive anchors that will be torqued, the minimum edge distance and spacing shall are given in Tables 6, 9, 12, 15 and 18 of this document.

For edge distances c_{ai} and anchor spacing s_{ai} the maximum torque T'_{max} shall comply with the following requirements:

Reduced Installation Torque T_{max} for Edge Distances c_{ai} < (5 x d)					
Edge Distance c _{ai}	Minimum Anchor Spacing, s _{ai}	= > Torque, T _{max}			
1.75 in. (45 mm)	5 x d ≤ s _{ai} < 16 in.	0.3 x T _{max}			
$\leq c_{ai} < 5 \times d$	s _{ai} ≥ 16 in. (406 mm)	0.5 x T _{max}			

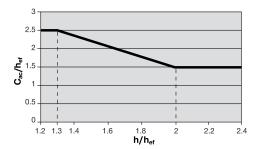
3.2.3.3.10. Critical Edge Distance, \mathbf{c}_{ac} : For the calculation of \mathbf{N}_{cb} , \mathbf{N}_{cbg} , \mathbf{N}_{a} and \mathbf{N}_{ag} in accordance with ACI 318 Section D.5.2.7 and Section 3.2.3.3.4 of this document, the critical edge distance, \mathbf{c}_{ac} , must be taken as follows:

i.
$$c_{ac} = 1.5 h_{ef}$$
 for $h/h_{ef} \ge 2$

ii.
$$c_{ac} = 2.5 h_{ef}$$
 for $h/h_{ef} \le 1.3$



For definition of h and $h_{\rm ef}$, see Figure 1 of this document.



Linear interpolation is permitted to determine the ratio $c_{\rm ac}/h_{\rm ef}$ for values of $h/h_{\rm ef}$ between 2 and 1.3 as illustrated in the graph above.

3.2.3.3.11. Design Strength in Seismic Design Categories C, D, E and F: In

structures assigned to Seismic Design Category C, D, E or F under the IBC or IRC, the design must be performed according to ACI 318 Section D.3.3, and the anchor strength must be adjusted in accordance with 2009 IBC Section 1908.1.9 or 2006 IBC Section 1908.1.16. For brittle steel elements, the anchor strength must be adjusted in accordance with ACI 318-05 D.3.3.5 or ACI 318-08 D.3.3.5 or D.3.3.6. The nominal steel shear strength, V_{sa} , must be adjusted by $\alpha_{_{\text{V,seis}}}$ as given in the tables summarized in Table 1a for the corresponding anchor steel. An adjustment of the nominal bond strength $\tau_{\text{\tiny k,cr}}$ by $\alpha_{\text{\tiny N,seis}}$ is not necessary, since $\alpha_{N.seis}$ = 1.0 in all cases.

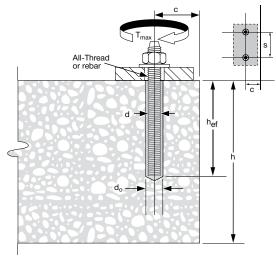
3.2.3.3.12. Interaction of Tensile and

Shear Forces: For designs that include combined tension and shear, the interaction of tension and shear loads must be calculated in accordance with ACI 318 D.7.



3.2.3.4 Technical Data

Figure 1—Installation Parameters



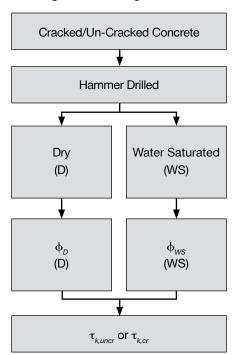
Threaded rod/reinforcing bar

Table 1a - Design Table Index

Design strength ¹		Threac	led rod	Deformed reinforcement bar			
		Fractional	Metric	U.S. (imperial)	EU (metric)	Canadian (metric)	
Steel	N _{sa} , V _{sa}	Table 5	Table 8	Table 11	Table 14	Table 17	
Concrete	N_{cb} , N_{cbg} , V_{cb} , V_{cbg} , V_{cp} , V_{cpg}	Table 6	Table 9	Table 12	Table 15	Table 18	
Bond ²	N _a , N _{ag}	Table 7	Table 10	Table 13	Table 16	Table 19	

¹ Design strengths are as set forth in ACI 318 D.4.1.2.

Figure 2 — Flowchart for Establishment of Design Bond Strength



 $^{2\,}$ See Section 3.2.3.3.4 of this document for bond strength information.



Table 1b — Example Allowable Stress Design Values for Illustrative Purposes

Nominal Anchor Diameter	Effective Embedment Depth	f'_c	k _{c,uncr}	α	Ф	Allowable Tension Load ΦΝ _n /α
d	h _{ef}					n,
(in)	(in)	(psi)	(-)	(-)	(-)	(lb)
3/8	2 3/8	2,500	24	1.48	0.65	1929
1/2	2 3/8	2,500	24	1.48	0.65	1929
5/8	3 1/8	2,500	24	1.48	0.65	2911
3/4	3 1/2	2,500	24	1.48	0.65	3451*
7/8	3 1/2	2,500	27	1.48	0.65	3882
1	4	2,500	27	1.48	0.65	4743

For SI: 1 lb = 4.45 kN, 1 psi = 0.00689 MPa, 1 in. = 25.4 mm, $^{\circ}$ C = $[(^{\circ}F) - 32]/1.8$

Design Assumptions:

- 1. Single anchor with static tension load only; ASTM A 193 Grade B7 threaded rod, ductile.
- 2. Vertical downward installation direction.
- 3. Inspection Regimen = Periodic.
- 4. Installation temperature = 14 104 °F.
- 5. Long term temperature = 75 °F.
- 6. Short term temperature = 104 °F.
- 7. Dry hole condition carbide drilled hole.
- 8. Embedment depth = $h_{ef min}$.
- 9. Concrete determined to remain uncracked for the life of the anchorage.
- 10. Load combination from ACI 318 Section 9.2 (no seismic loading).
- 11. 30 percent Dead Load (D) and 70 percent Live Load (L); Controlling load combination 1.2 D + 1.6 L.
- 12. Calculation of α based on weighted average: α = 1.2 D + 1.6 L = 1.2 (0.30) +1.6 (0.70) = 1.48.
- 13. Normal weight concrete: $f_c = 2,500 \text{ psi}$
- 14. Edge distance: $c_{a1} = c_{a2} > c_{ac}$
- 15. Member thickness: h ≥ h_{min}.

^{*} Verify capacity

Capacity	ACI 318 reference	Formula	Calculation	Ф	ΦN _n
Steel	D.5.1	$N_{sa} = nA_{se, N} f_{uta}$	$N_{sa} = 0.3345 \cdot 125,000$	0.75	31,360 lb
Concrete	D.5.2	$N_{cb} = k_{c,uncr} (f'_c)^{0.5} h_{ef}^{1.5}$	$N_{cb} = 24 \cdot (2,500)^{0.5} \cdot 3^{1.5}$	0.65	5,107 lb
Bond	D.5.3**	$N_a = \pi d h_{ef} \tau_{k,uncr}$	$N_a = \pi \cdot 3/4 \cdot 3.5 \cdot 1,710$	0.65	9,166 lb

Concrete breakout is decisive; hence the ASD value will be calculated as $\frac{5,107 \text{ lb}}{1.48}$ = 3,451 lb

^{**} Design equation provided in Section 3.2.3.3.4 as new section ACI 318 D.5.3.9, Eq. (D-16f).



Table 2 — Tensile Properties of Common Carbon Steel Threaded Rod Materials¹

Threaded Rod Specification		$\begin{array}{c} \text{Minimum} \\ \text{Specified} \\ \text{Ultimate} \\ \text{Strength} \\ f_{\text{uta}} \end{array}$	$\begin{array}{c} \text{Minimum} \\ \text{Specified Yield} \\ \text{Strength 0.2\%} \\ \text{Offset} \\ f_{\text{ya}} \end{array}$	$f_{ m uta}/f_{ m ya}$	Minimum Elongation, Percent ⁵	Minimum Reduction of Area, Percent	Specification for Nuts ⁶
ASTM A 193 ² Grade B7 ≤ 2-1/2 in (≤ 64 mm)	psi (MPa)	125,000 (860)	105,000 (725)	1.19	16	50	ASTM A194
ASTM F 568M³ Class 5.8 M5 (1/4 in) to M24 (1 in) (equivalent to ISO 898-1)	MPa (psi)	500 (72,500)	400 (58,000)	1.25	10	35	DIN 934 (8-A2K) ASTM A563 Grade DH ⁷
ISO 898-1 ⁴ Class 5.8	898-1 ⁴ Class 5.8 MPa (psi)		400 (58,000)	1.25	22	-	DIN 934 (Grade 6)
ISO 898-1 ⁴ Class 8.8	MPa (psi)	800 (116,000)	640 (92,800)	1.25	12	52	DIN 934 (Grade 8)

¹ Hilti HIT-HY 150 MAX-SD adhesive may be used in conjunction with all grades of continuously threaded carbon steel rod (all-thread) that comply with the code reference standards and that have thread characteristics comparable with ANSI B1.1 UNC Coarse Thread Series or ANSI B1.13M M Profile Metric Thread Series. Values for threaded rod types and associated nuts supplied by Hilti are provided here.

- 2 Standard Specification for Alloy-Steel and Stainless Steel Bolting Materials for High-Temperature Service
- 3 Standard Specification for Carbon and Alloy Steel Externally Threaded Metric Fasteners
- 4 Mechanical properties of fasteners made of carbon steel and alloy steel Part 1: Bolts, screws and studs
- 5 Based on 2-in. (50 mm) gauge length except ASTM A 193, which are based on a gauge length of 4d and ISO 898 which is based on 5d.
- 6 Nuts of other grades and styles having specified proof load stresses greater than the specified grade and style are also suitable. Nuts must have specified proof load stresses equal to or greater than the minimum tensile strength of the specified threaded rod.
- 7 Nuts for fractional rods.

Table 3 —Tensile Properties of Common Stainless Steel Threaded Rod Materials¹

Threaded Rod Specification		$\begin{array}{c} \text{Minimum} \\ \text{Specified} \\ \text{Ultimate} \\ \text{Strength} \\ f_{\text{uta}} \end{array}$	$\begin{array}{c} \text{Minimum} \\ \text{Specified Yield} \\ \text{Strength 0.2\%} \\ \text{Offset} \\ f_{\text{ya}} \end{array}$	$f_{ m uta}/f_{ m ya}$	Minimum Elongation, Percent ⁵	Minimum Reduction of Area, Percent	Specification for Nuts ⁴
ASTM F 593 ² CW1 (316) 1/4 to 5/8 in	psi (MPa)	100,000 (690)	65,000 (450)	1.54	20	-	F 594
ASTM F 593 ² CW2 (316) 3/4 to 1-1/2 in	psi (MPa)	85,000 (585)	45,000 (310)	1.89 25		-	F 594
ISO 3506-1 ³ A4-70 M8 – M24	MPa (psi)	700 (101,500)	450 (65,250)	1.56 40 -		ISO 4032	

¹ Hilti HIT-HY 150 MAX-SD may be used in conjunction with all grades of continuously threaded stainless steel rod (all-thread) that comply with the code reference standards and that have thread characteristics comparable with ANSI B1.1 UNC Coarse Thread Series or ANSI B1.13M M Profile Metric Thread Series. Values for threaded rod types and associated nuts supplied by Hilti are provided here.

- 2 Standard Steel Specification for Stainless Steel Bolts, Hex Cap Screws, and Studs
- 3 Mechanical properties of corrosion-resistant stainless steel fasteners Part 1: Bolts, screws and studs
- 4 Nuts of other grades and styles having specified proof load stresses greater than the specified grade and style are also suitable. Nuts must have specified proof load stresses equal to or greater than the minimum tensile strength of the specified threaded rod.



Table 4 — Tensile Properties of Common Reinforcing Bars

Reinforcing Bar Specification		Minimum Specified Ultimate Strength $f_{\scriptscriptstyle ext{uta}}$	Minimum specified yield strength $f_{_{ m ya}}$
ASTM A 615 ¹ Gr. 60	psi	90,000	60,000
	(MPa)	(620)	(415)
ASTM A 615 ¹ Gr. 40	psi	60,000	40,000
	(MPa)	(415)	(275)
DIN 488 ² BSt 500	MPa	550	500
	(psi)	(79,750)	(72,500)
CAN/CSA-G30.18 ³ Gr. 400	MPa	540	400
	(psi)	(78,300)	(58,000)

¹ Standard Specification for Deformed and Plain Carbon Steel Bars for Concrete Reinforcement

² Reinforcing steel; reinforcing steel bars; dimensions and masses

³ Billet-Steel Bars for Concrete Reinforcement



Table 5 — Steel Design Information for Fractional Threaded Rod¹

D	in lafa maratica	Courada a l	Ulaita			Nominal rod	diameter (in)			
Design Information		Symbol	Units	3/8	1/2	5/8	3/4	7/8	1	
Das	100	-1	in	0.375	0.5	0.625	0.75	0.875	1	
HOC	d O.D.	d	(mm)	(9.5)	(12.7)	(15.9)	(19.1)	(22.2)	(25.4)	
Roc	d effective cross-sectional	_	in²	0.0775	0.1419	0.2260	0.3345	0.4617	0.6057	
area	a	A _{se}	(mm²)	(50)	(92)	(146)	(216)	(298)	(391)	
		N	lbf	5,620	10,290	16,385	24,250	33,470	43,910	
	Nominal strength as governed by steel	N _{sa}	(kN)	(25.0)	(45.8)	(72.9)	(107.9)	(148.9)	(195.3)	
5.8	strength	V	lbf	2,810	6,175	9,830	14,550	20,085	26,345	
ass	Strongth	V _{sa}	(kN)	(12.5)	(27.5)	(43.7)	(64.7)	(89.3)	(117.2)	
SO 898-1 Class 5.8	Reduction for seismic shear	α _{V,seis}	-		0.70					
SO 86	Strength reduction factor Φ for tension ²	Ф	-		0.65					
	Strength reduction factor Φ for shear ²	Ф	ı	0.60						
	Nominal strength as governed by steel strength	N _{sa}	lbf	9,690	17,740	28,250	41,810	57,710	75,710	
			(kN)	(43.1)	(78.9)	(125.7)	(186.0)	(256.7)	(336.8)	
B7		V	lbf	4,845	10,640	16,950	25,090	34,630	45,425	
ස		V _{sa}	(kN)	(21.5)	(47.3)	(75.4)	(111.6)	(154.0)	(202.1)	
ASTM A 193	Reduction for seismic shear	α _{V,seis}	-			0.	70			
AST	Strength reduction factor Φ for tension ³	Ф	-			0.	75			
	Strength reduction factor Φ for shear ³	Ф	-			0.	65			
		N	lbf	7,750	14,190	22,600	28,430	39,245	51,485	
SSS	Nominal strength	N _{sa}	(kN)	(34.5)	(63.1)	(100.5)	(126.5)	(174.6)	(229.0)	
ainle	as governed by steel strength	V	lbf	3,875	8,515	13,560	17,060	23,545	30,890	
/ St		V _{sa}	(kN)	(17.2)	(37.9)	(60.3)	(75.9)	(104.7)	(137.4)	
93, CM	Reduction for seismic shear	α _{V,seis}	-			0.	70			
ASTM F593, CW Stainless	Strength reduction factor Φ for tension ²	Ф	-			0.	65			
AS	Strength reduction factor Φ for shear ²	Ф	-	0.60						

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

¹ Values provided for common rod material types based on published strengths and calculated in accordance with ACI 318 Eq. (D-3) and Eq. (D-20). Other material specifications are admissible, subject to the approval of the code official. Nuts and washers must be appropriate for the rod strength.

² For use with the load combinations of IBC Section 1605.2.1, or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of Φ must be determined in accordance with ACI 318 D.4.5. Values correspond to a brittle steel element.

³ For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of Φ must be determined in accordance with ACI 318 D.4.5. Values correspond to a ductile steel element.



Table 6 — Concrete Breakout Design Information for Fractional Threaded Rod¹

Design Information	Cumbal	Lloito			Nominal rod	diameter (in)			
Design Information	Symbol	Units	3/8	1/2	5/8	3/4	7/8	1	
Effectiveness factor for	۷.	in-lb	24	24	24	24	27	27	
uncracked concrete	k _{c,uncr}	(SI)	(10)	(10)	(10)	(10)	(11.3)	(11.3)	
Effectiveness factor for	k	in-lb	17	17	17	17	17	17	
cracked concrete	k _{c,cr}	(SI)	(7)	(7)	(7)	(7)	(7)	(7)	
Minimum anchor spacing ⁴		in	1-7/8	2-1/2	3-1/8	3-3/4	4-3/8	5	
Willimitan anchor spacing	S _{min}	(mm)	(48)	(64)	(79)	(95)	(111)	(127)	
Minimum edge distance ⁴		in	1-7/8	2-1/2	3-1/8	3-3/4	4-3/8	5	
Williman eage distance	C _{min}	(mm)	(48)	(64)	(79)	(95)	(111)	(127)	
NA::		in	h _{ef} +	1-1/4		b .	04 (3)		
Minimum member thickness	h _{min}	(mm)	(h _{ef}	+ 30)		h _{ef} +	20,0		
Critical edge distance — splitting (for uncracked concrete)	C _{ac}	-		See S	Section 3.2.3.3.	10 of this docu	ıment.		
Strength reduction factor for tension, concrete failure modes, Condition B ²	Ф	-			0.	65			
Strength reduction factor for shear, concrete failure modes, Condition B ²	Ф	-			0.70				

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

- 1 For additional setting information, see installation instructions in Figure 5.
- 2 Values provided for post-installed anchors with category as determined from ACI 355.2 given for Condition B. Condition B applies without supplementary reinforcement or where pullout (bond) or pryout govern, as set forth in ACI 318 D.4.4, while condition A requires supplemental reinforcement. Values are for use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of Φ must be determined in accordance with ACI 318 D.4.5.
- 3 d_0 = hole diameter.
- 4 For installations with a 1-3/4 in. edge distance, the installation torque must be reduced. Please refer to section 3.2.3.3.9.



Table 7 — Bond Strength Design Information for Fractional Threaded Rod¹

Dania	n Info	ormation	Cumbal	Units		N	ominal rod	diameter (i	in)	
Desig	n inic	ormation	Symbol	Units	3/8	1/2	5/8	3/4	7/8	1
		Characteristic bond strength	_	psi	1,985	1,985	1,850	1,710	1,575	1,440
	A	in uncracked concrete	$ au_{ ext{k,uncr}}$	(MPa)	(13.7)	(13.7)	(12.7)	(11.8)	(10.9)	(9.9)
	^	Characteristic bond strength	_	psi	696	763	821	881	889	896
Je ²		in cracked concrete ³	$ au_{k,cr}$	(MPa)	(4.8)	(5.3)	(5.7)	(6.1)	(6.1)	(6.2)
ranç		Characteristic bond strength	τ	psi	1,610	1,610	1,495	1,385	1,275	1,170
a. n	В	in uncracked concrete	$ au_{ ext{k,uncr}}$	(MPa)	(11.1)	(11.1)	(10.3)	(9.6)	(8.8)	(8.1)
erati		Characteristic bond strength		psi	561	615	662	711	717	723
Temperature range ²		in cracked concrete ³	$ au_{k,cr}$	(MPa)	(3.9)	(4.2)	(4.6)	(4.9)	(4.9)	(5.0)
<u>l</u>		Characteristic bond strength in uncracked concrete	_	psi	930	930	865	805	740	675
	С		$ au_{ ext{k,uncr}}$	(MPa)	(6.4)	(6.4)	(6.0)	(5.5)	(5.1)	(4.7)
		Characteristic bond strength	τ	psi	321	352	379	407	410	414
		in cracked concrete ³	$ au_{k,cr}$	(MPa)	(2.2)	(2.4)	(2.6)	(2.8)	(2.8)	(2.9)
Minim	ium a	nchor embedment depth	h	in.	2-3/8	2-3/4	3-1/8	3-1/2	3-1/2	4
			h _{ef,min}	(mm)	(60)	(70)	(79)	(89)	(89)	(102)
Maxin	num a	anchor embedment depth	h	in.	7-1/2	10	12-1/2	15	17-1/2	20
			h _{ef,max}	(mm)	(191)	(254)	(318)	(381)	(445)	(508)
Permissible installation	itions	concrete	Anchor Category	-			-	1		
Permi	cond		Ф _d & Ф _{ws}				0.	65		

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

- 1 Bond strength values correspond to concrete compressive strength range 2,500 psi ≤ f' ≤ 4,500 psi. For 4,500 psi < f' ≤ 6,500 psi, tabulated characteristic bond strengths may be increased by 6 percent. For 6,500 psi < f' ≤ 8,000 psi, tabulated characteristic bond strengths may be increased by 10 percent.</p>
- 2 Temperature range A: Maximum short term temperature = 104°F (40°C), maximum long term temperature = 75°F (24°C). Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C). Temperature range C: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 162°F (72°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

3 For structures assigned to Seismic Design Categories C, D, E or F, bond strength values are multiplied by $\alpha_{Nseis} = 1.0 = 0$ no reduction.



Table 8 — Steel Design Information for Metric Threaded Rod¹

Dagia	n Information	Cymphol	l leite		Nomir	nal rod diamete	r (mm)				
Desig	n Information	Symbol	Units	10	12	16	20	24			
D- 4 (-1	mm	10	12	16	20	24			
Rod (J.D.	d	(in)	(0.39)	(0.47)	(0.63)	(0.79)	(0.94)			
D1-	effective consequently and	_	mm²	58	84.3	157	245	353			
HOO 6	effective cross-sectional area	A _{se}	(in²)	(0.090)	(0.131)	(0.243)	(0.380)	(0.547)			
		N	kN	29.0	42.2	78.5	122.5	176.5			
5.8	Nominal strength as governed	N _{sa}	(lbf)	(6,520)	(9,475)	(17,650)	(27,540)	(39,680)			
Class (by steel strength		kN	14.5	25.3	47.1	73.5	105.9			
Ö		V _{sa}	(lbf)	(3,260)	(5,685)	(10,590)	(16,525)	(23,810)			
SO 898-1	Reduction for seismic shear	α _{V,seis}	-			0.70					
<u>S</u>	Strength reduction factor Φ for tension ²	Ф	-			0.65					
	Strength reduction factor Φ for shear ²	Ф	-		0.60						
	Nominal strength as governed by steel strength	N	kN	46.4	67.4	125.6	196.0	282.4			
3.8		N _{sa}	(lbf)	(10,430)	(15,160)	(28,235)	(44,065)	(63,485)			
		\/	kN	23.2	40.5	75.4	117.6	169.4			
œ.		V _{sa}	(lbf)	(5,215)	(9,100)	(16,940)	(26,440)	(38,090)			
898-1 CI.	Reduction for seismic shear	α _{V,seis}	-			0.70					
8 OSI	Strength reduction factor Φ for tension ²	Ф	-			0.65					
	Strength reduction factor Φ for shear ²	Ф	-			0.60					
		.	kN	40.6	59.0	109.9	171.5	247.1			
လိ	Nominal strength as governed	N _{sa}	(lbf)	(9,130)	(13,263)	(24,703)	(38,555)	(55,550)			
Ą.	by steel strength		kN	20.3	35.4	65.9	102.9	148.3			
<u>۲</u> .		V _{sa}	(lbf)	(4,565)	(7,960)	(14,825)	(23,135)	(33,330)			
3506-1 Cl. A4 SS ³	Reduction for seismic shear	α _{,seis}	-			0.70					
ISO 3	Strength reduction factor Φ for tension ²	Φ	-			0.65					
<u>Ō</u>	Strength reduction factor Φ for shear ²	Ф	-			0.60					

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

3 A4-70 Stainless (M10 - M24 diameters)

¹ Values provided for common rod material types based on published strengths and calculated in accordance with ACI 318 Eq. (D-3) and Eq. (D-20). Other material specifications are admissible, subject to the approval of the code official. Nuts and washers must be appropriate for the rod strength.

² For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of f must be determined in accordance with ACI 318 D.4.5. Values correspond to a brittle steel element.



Table 9 — Concrete Breakout Design Information for Metric Threaded Rod¹

Decient Information	C: male al	l laita		Nomi	nal rod diameter	(mm)		
Design Information	Symbol		20	24				
Effectiveness factor	le.	SI	10	10	10	10	11.3	
for uncracked concrete	k _{c,uncr}	(in-lb)	(24)	(24)	(24)	(24)	(27)	
Effectiveness factor	le.	SI	7	7	7	7	7	
for cracked concrete	k _{c,cr}	(in-lb)	(17)	(17)	(17)	(17)	(17)	
Minimum anabar anasina4		mm	50	60	80	100	120	
Minimum anchor spacing ⁴	S _{min}	(in)	(2.0)	(2.4)	(3.2)	(3.9)	(4.7)	
Minimum adag diatangga		mm	50	60	80	100	120	
Minimum edge distance⁴	C _{min}	(in)	(2.0)	(2.4)	(3.2)	(3.9)	(4.7)	
Minimum member thickness	4	mm	h _{ef} + 30		h i	Od (3)		
Willimum member trickness	h _{min}	(in)	(h _{ef} + 1-1/4)		n _{ef} +	20 ₀ (4)		
Critical edge distance — splitting		_		See Section	3 2 3 3 10 of thi	s document		
(for uncracked concrete)	C _{ac}	-		See Section	3.2.3.3.10 01 1111	s document.		
Strength reduction factor for tension,	Φ	-		0.65				
concrete failure modes, Condition B ²								
Strength reduction factor for shear, concrete failure modes, Condition B ²	Ф	-		0.70				

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa

- 1 For additional setting information, see installation instructions in Figure 5.
- 2 Values provided for post-installed anchors with category as determined from ACI 355.2 given for Condition B. Condition B applies without supplementary reinforcement or where pullout (bond) or pryout govern, as set forth in ACI 318 D.4.4, while condition A requires supplemental reinforcement. Values are for use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of Φ must be determined in accordance with ACI 318 D.4.5.
- 3 d_0 = drill bit diameter.
- 4 For installations with a 1-3/4 in. edge distance, the installation torque must be reduced. Please refer to section 3.2.3.3.9.



Table 10 — Bond Strength Design Information for Metric Threaded Rod¹

Design Inf	O K100 O	*:an	Cumbal	Units		Nomina	l rod diamet	er (mm)	
Design Inf	oma	tion	Symbol	Units	10	12	16	20	24
		Characteristic bond strength		MPa	13.7	13.7	12.7	11.8	10.9
	,	in uncracked concrete	$ au_{ ext{k,uncr}}$	(psi)	(1,985)	(1,985)	(1,850)	(1,710)	(1,575)
	A	Characteristic bond strength		MPa	4.9	5.1	5.7	6.1	6.2
ge ²		in cracked concrete ³	$ au_{k,cr}$	(psi)	(705)	(744)	(822)	(884)	(893)
ran		Characteristic bond strength	_	MPa	11.1	11.1	10.3	9.6	8.8
inre	В	in uncracked concrete	$ au_{ ext{k,uncr}}$	(psi)	(1,610)	(1,610)	(1,500)	(1,390)	(1,275)
erat		Characteristic bond strength	τ.	MPa	3.9	4.1	4.6	4.9	5.0
Temperature range²		in cracked concrete ³	τ _{k,cr}	(psi)	(569)	(600)	(663)	(712)	(720)
"		Characteristic bond strength	τ _{k,uncr}	MPa	6.4	6.4	6.0	5.5	5.1
	С	in uncracked concrete		(psi)	(930)	(930)	(865)	(805)	(740)
		Characteristic bond strength	τ	MPa	2.2	2.4	2.6	2.8	2.8
		in cracked concrete ³	$ au_{k,cr}$	(psi)	(326)	(343)	(379)	(408)	(412)
Minimum	anch	or embedment depth	h	mm	60	70	80	90	96
			h _{ef,min}	(in.)	(2.4)	(2.8)	(3.1)	(3.5)	(3.8)
Maximum	anch	nor embedment depth	h	mm	200	240	320	400	480
			h _{ef,max}	(in.)	(7.9)	(9.4)	(12.6)	(15.7)	(18.9)
ssible ation ions	Dry	concrete and	Anchor Category	-			1		
Permissible installation conditions	Wa	ter-saturated concrete	Ф _d & Ф _{ws}	-			0.65		

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

- 1 Bond strength values correspond to concrete compressive strength range 2,500 psi ≤ f' ≤ 4,500 psi. For 4,500 psi < f' ≤ 6,500 psi, tabulated characteristic bond strengths may be increased by 6 percent. For 6,500 psi < f' ≤ 8,000 psi, tabulated characteristic bond strengths may be increased by 10 percent.</p>
- 2 Temperature range A: Maximum short term temperature = 104°F (40°C), maximum long term temperature = 75°F (24°C). Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C). Temperature range C: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 162°F (72°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

3 For structures assigned to Seismic Design Categories C, D, E or F, bond strength values are multiplied by $\alpha_{N,seis} = 1.0 \Rightarrow no$ reduction.



Table 11 — Steel Design Information for U.S. Imperial Reinforcing Bars¹

						Bar	Size		
Des	ign Information	Symbol	Units	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8
Nor	ninal bar diameter	d	in.	3/8	1/2	5/8	3/4	7/8	1
1401	milai bai diametei	u u	(mm)	(9.5)	(12.7)	(15.9)	(19.1)	(22.2)	(25.4)
Bar	effective cross-sectional area	A _{se}	in.²	0.11	0.2	0.31	0.44	0.6	0.79
Dai	chective cross sectional area	Se	(mm²)	(71)	(129)	(200)	(284)	(387)	(510)
		N _{sa}	lb	6,600	12,000	18,600	26,400	36,000	47,400
40	Nominal strength as governed	sa	(kN)	(29.4)	(53.4)	(82.7)	(117.4)	(160.1)	(210.9)
Ģ.	by steel strength	\ \ <u>\</u>	lbf	3,960	7,200	11,160	15,840	21,600	28,440
615		V _{sa}	(kN)	(17.6)	(32.0)	(49.6)	(70.5)	(96.1)	(126.5)
ASTM A 6	Reduction for seismic shear	α _{V,seis}	-			0.	70		
AS	Strength reduction factor Φ for tension ²	Ф	-			0.	65		
	Strength reduction factor Φ for shear ²	Ф	-			0.	60		
		NI NI	lb	9,900	18,000	27,900	39,600	54,000	71,100
	Nominal strength as governed	N _{sa}	(kN)	(44.0)	(80.1)	(124.1)	(176.2)	(240.2)	(316.3)
Gr. 60	by steel strength	V	lb	5,940	10,800	16,740	23,760	32,400	42,660
615 G		V _{sa}	(kN)	(26.4)	(48.0)	(74.5)	(105.7)	(144.1)	(189.8)
ASTM A 61	Reduction for seismic shear	α _{V,seis}	-			0.	70		
AS	Strength reduction factor f for tension ²	Ф	-			0.	65		
	Strength reduction factor f for shear ²	Ф	-			0.	60		

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

¹ Values provided for common rod material types based on published strengths and calculated in accordance with ACI 318 Eq. (D-3) and Eq. (D-20). Other material specifications are admissible, subject to the approval of the code official. Nuts and washers must be appropriate for the rod strength.

² For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of f must be determined in accordance with ACI 318 D.4.5. Values correspond to a brittle steel element.



Table 12 — Concrete Breakout Design Information for U.S. Imperial Reinforcing Bars¹

Decise Information	Cumbal	Lloito			Bar	Size		
Design Information	Symbol	Units	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8
Effectiveness factor for uncracked concrete	le.	in-lb	24	24	24	24	24	24
Effectiveness factor for uncracked concrete	k _{c,uncr}	(SI)	(10)	(10)	(10)	(10)	(10)	(10)
Effectiveness factor for cracked concrete	le .	in-lb	17	17	17	17	17	17
Effectiveness factor for cracked concrete	k _{c,cr}	(SI)	(7)	(7)	(7)	(7)	(7)	(7)
Minimum bar spacing ⁴		in.	1-7/8	2-1/2	3-1/8	3-3/4	4-3/8	5
Willimum bar spacing	S _{min}	(mm)	(48)	(64)	(79)	(95)	(111)	(127)
∕linimum edge distance⁴		in.	1-7/8	2-1/2	3-1/8	3-3/4	4-3/8	5
Millimum eage distance	C _{min}	(mm)	(48)	(64)	(79)	(95)	(111)	(127)
Minimum member thickness	h	in.	h _{ef} +	1-1/4		b ±	24 (3)	
William member unckness	h _{min}	(mm)	(h _{ef} -	+ 30)		h _{ef} +	2u ₀ (*)	
Critical edge distance — splitting	C _{ac}	_		See Sect	ion 3 2 3 3	10 of this do	ocument	
(for uncracked concrete)	ac							
Strength reduction factor for tension, concrete failure modes, Condition B ²	Ф	-	0.65					
Strength reduction factor for shear, concrete failure modes, Condition B ²	Ф	-	0.70					

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

- 1 For additional setting information, see installation instructions in Figure 5.
- 2 Values provided for post-installed anchors with category as determined from ACI 355.2 given for Condition B. Condition B applies without supplementary reinforcement or where pullout (bond) or pryout govern, as set forth in ACI 318 D.4.4, while condition A requires supplemental reinforcement. Values are for use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of f must be determined in accordance with ACI 318 D.4.5.
- 3 d_0 = drill bit diameter.
- 4 For installations with a 1-3/4 in. edge distance, the installation torque must be reduced. Please refer to section 3.2.3.3.9.



Table 13 — Bond Strength Design Information for U.S. Imperial Reinforcing Bars¹

Dasia	n Info	avecation.	Cumbal	Units			Bar	Size			
Desig	n inic	ormation	Symbol	Units	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	
		Characteristic bond strength in uncracked concrete	$ au_{ ext{k,uncr}}$	psi MPa				.9)			
Φ ²	A	Characteristic bond strength in cracked concrete ³	$ au_{ ext{k,cr}}$	psi MPa	696 (4.8)	763 (5.3)	821 (5.7)	881 (6.1)	889 (6.1)	896 (6.2)	
ıre rang		Characteristic bond strength in uncracked concrete	$ au_{ ext{k,uncr}}$	psi MPa)45 .2)			
Temperature range ²	В	Characteristic bond strength in cracked concrete ³	$ au_{k,cr}$	psi MPa	561 (3.9)	615 (4.2)	662 (4.6)	711 (4.9)	717 (4.9)	723 (5.0)	
Ter		Characteristic bond strength in uncracked concrete	$ au_{ ext{k,uncr}}$	psi MPa		605 (4.2)					
	С	Characteristic bond strength in cracked concrete ³	$ au_{k,cr}$	psi MPa	321 (2.2)	352 (2.4)	379 (2.6)	407 (2.8)	410 (2.8)	414 (2.9)	
Minim	ium a	nchor embedment depth	h _{ef,min}	in. (mm)	2-3/8 (60)	2-3/4 (70)	3-1/8 (79)	3-1/2 (89)	3-1/2 (89)	4 (102)	
Maxin	num a	anchor embedment depth	h _{ef,max}	in. (mm)	7-1/2 (191)	10 (254)	12-1/2 (318)	15 (381)	17-1/2 (445)	20 (508)	
Permissible installation	conditions	Dry concrete and Water-saturated	Anchor Category	-				1			
Permi	cond	concrete	$\Phi_{d} \Phi f_{ws}$		0.65						

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

- 1 Bond strength values correspond to concrete compressive strength range 2,500 psi $\leq f' \leq 4,500$ psi. For 4,500 psi $< f' \leq 6,500$ psi, tabulated characteristic bond strengths may be increased by 6 percent. For 6,500 psi $< f' \leq 8,000$ psi, tabulated characteristic bond strengths may be increased by 10 percent.
- 2 Temperature range A: Maximum short term temperature = 104°F (40°C), maximum long term temperature = 75°F (24°C). Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C). Temperature range C: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 162°F (72°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

3 For structures assigned to Seismic Design Categories C, D, E or F, bond strength values are multiplied by $\alpha_{N,seis} = 1.0 = 0$ no reduction.



Table 14 — Steel Design Information for EU Metric Reinforcing Bars¹

Dad	ica Information	Cumbal	Units			Bar	Size			
Des	sign Information	Symbol	Units	10	12	14	16	20	25	
No	ninal bar diameter	d	mm	10.0	12.0	14.0	16.0	20.0	25.0	
INOI	milai bai diametei	u	(in.)	(0.394)	(0.472)	(0.551)	(0.630)	(0.787)	(0.984)	
Do	effective cross-sectional area	_	mm²	78.5	113.1	153.9	201.1	314.2	490.9	
Dar	enective cross-sectional area	A _{se}	(in.²)	(0.122)	(0.175)	(0.239)	(0.312)	(0.487)	(0.761)	
		NI NI	kN	43.2	62.2	84.7	110.6	172.8	270.0	
8	Nominal strength as governed by	N _{sa}	(lb)	(9,710)	(13,985)	(19,035)	(24,860)	(38,845)	(60,695)	
550/500	steel strength	V	kN	25.9	37.3	50.8	66.4	103.7	162.0	
St 56		V _{sa}	(lb)	(5,830)	(8,390)	(11,420)	(14,915)	(23,310)	(36,415)	
1488 BSt	Reduction for seismic shear	α _{V,seis}	-	0.70						
N N	Strength reduction factor Φ for tension ²	Ф	-	0.65						
	Strength reduction factor Φ for shear ²	Ф	-	0.60						

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

- 1 Values provided for common rod material types based on published strengths and calculated in accordance with ACI 318 Eq. (D-3) and Eq. (D-20). Other material specifications are admissible, subject to the approval of the code official. Nuts and washers must be appropriate for the rod strength.
- 2 For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of f must be determined in accordance with ACI 318 D.4.5. Values correspond to a brittle steel element.



Table 15 — Concrete Breakout Design Information for EU Metric Reinforcing Bars¹

Design Information	Sumbol	Lloito			Bar	size				
Design Information	Symbol	Units	10	12	14	16	20	25		
Effectiveness factor for uncracked concrete	le.	SI			10			12.6		
Effectiveness factor for uncracked concrete	k _{c,uncr}	(in-lb)			(24)			(30)		
Effectiveness factor for cracked concrete	le.	SI			-	7				
Effectiveness factor for cracked concrete	k _{c,cr}	(in-lb)			(1	7)				
Minimum har angoing ⁴		mm	50	60	70	80	100	125		
Minimum bar spacing⁴	S _{min}	(in.)	(2)	(2.4)	(2.8)	(3.1)	(3.9)	(4.9)		
Minimum adae dietanee4		mm	50	60	70	80	100	125		
Minimum edge distance⁴	C _{min}	(in.)	(2)	(2.4)	(2.8)	(3.1)	(3.9)	(4.9)		
Minimum member thickness	h	mm		+ 30		b ±	24 (3)			
Minimum member unckness	h _{min}	(in.)	(h _{ef} +	1-1/4)		h _{ef} +	20 ₀ (4)			
Critical edge distance — splitting		_		See Sec	stion 3 2 3 3	10 of this do	cument			
(for uncracked concrete)	C _{ac}	_		366 360	,11011 3.2.3.3.	10 01 11115 00	Cument.			
Strength reduction factor for tension,	Ф	_			0.65					
concrete failure modes, Condition B ²										
Strength reduction factor for shear,	Ф	_			0.70					
concrete failure modes, Condition B ²	·		3.70							

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

- 1 For additional setting information, see installation instructions in Figure 5.
- 2 Values provided for post-installed anchors with category as determined from ACI 355.2 given for Condition B. Condition B applies without supplementary reinforcement or where pullout (bond) or pryout govern, as set forth in ACI 318 D.4.4, while condition A requires supplemental reinforcement. Values are for use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of f must be determined in accordance with ACI 318 D.4.5.
- 3 d_0 = drill bit diameter.
- 4 For installations with a 1-3/4 in. edge distance, the installation torque must be reduced. Please refer to section 3.2.3.3.9.



Table 16 — Bond Strength Design Information for EU Metric Reinforcing Bars¹

Dooig	n Info	ormation	Symbol	Units			Bar	Size			
Desig	11 11110	omation	Symbol	UTIILS	10	12	14	16	20	25	
		Characteristic bond strength	_	MPa			8	.9			
	A	in uncracked concrete	$ au_{k,uncr}$	(psi)			(1,2	290)			
	^	Characteristic bond strength	_	MPa	4.9	5.1	5.4	5.7	6.1	6.1	
$\frac{1}{2}$		in cracked concrete ³	$ au_{k,cr}$	(psi)	(705)	(744)	(783)	(822)	(884)	(895)	
Temperature range ²		Characteristic bond strength	_	MPa			7	.2			
<u>le</u>	В	in uncracked concrete	τ _{k,uncr}	(psi)	(1,045)						
eratı		Characteristic bond strength		MPa	3.9	4.1	4.4	4.6	4.9	5.0	
πре		in cracked concrete ³	$ au_{k,cr}$	(psi)	(569)	(600)	(631)	(663)	(712)	(722)	
<u>=</u>		Characteristic bond strength	_	MPa			4	.2			
	С	in uncracked concrete	$ au_{k,uncr}$	(psi)			(60	05)			
	-	Characteristic bond strength	_	MPa	2.2	2.4	2.5	2.6	2.8	2.9	
		in cracked concrete ³	$ au_{k,cr}$	(psi)	(326)	(343)	(361)	(379)	(408)	(413)	
Minim	ium a	nchor embedment depth	h	mm	60	70	75	80	90	100	
			h _{ef,min}	(in.)	(2.4)	(2.8)	(3.0)	(3.1)	(3.5)	(3.9)	
Maxin	num a	anchor embedment depth	h	mm	200	240	280	320	400	500	
			h _{ef,max}	(in.)	(7.9)	(9.4)	(11.0)	(12.6)	(15.7)	(19.7)	
ssible	tions	Dry concrete and	Anchor Category	-			-	1			
Permissible installation	conditions	Water-saturated concrete	Ф _d & Ф _{ws}	-			0.	65			

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

- 1 Bond strength values correspond to concrete compressive strength range 2,500 psi $\leq f' \leq 4,500$ psi. For 4,500 psi $< f' \leq 6,500$ psi, tabulated characteristic bond strengths may be increased by 6 percent. For 6,500 psi $< f' \leq 8,000$ psi, tabulated characteristic bond strengths may be increased by 10 percent.
- 2 Temperature range A: Maximum short term temperature = 104°F (40°C), maximum long term temperature = 75°F (24°C). Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C). Temperature range C: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 162°F (72°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

3 For structures assigned to Seismic Design Categories C, D, E or F, bond strength values are multiplied by $\alpha_{N,seis} = 1.0 = 0$ no reduction.



Table 17 — Steel Design Information for Canadian Metric Reinforcing Bars¹

*

Doc	sign Information	Symbol	Units		Bar	Size			
Des	ign mornation	Symbol	Units	10 M	15 M	20 M 19.5 (0.768) 298.6 (0.463) 161.3 (36,255) 96.8 (21,755)	25 M		
Nor	minal bar diameter	d	mm	11.3	16.0	19.5	25.2		
INOI	Tilital bai diametei	u	(in.)	(0.445)	(0.630)	(0.768)	(0.992)		
Bar	effective cross-sectional area	_	mm²	100.3	201.1	298.6	498.8		
Dai	enective cross-sectional area	A _{se}	(in.²)	(0.155)	(0.312)	(0.463)	(0.773)		
		NI NI	kN	54.2	108.6	161.3	269.3		
o	Nominal strength as governed	N _{sa}	(lb)	(12,175)	(24,410)	(36,255)	(60,550)		
Gr.400	by steel strength	V	kN	32.5	65.1	96.8	161.6		
		V _{sa}	(lb)	(7,305)	(14,645)	(21,755)	(36,330)		
r-G30.18	Reduction for seismic shear	α _{V,seis}	-		0.7	70			
CSA	Strength reduction factor f for tension ²	α	-		0.6	65			
	Strength reduction factor f for shear ² \qquad \qquad \qquad -				0.60				

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

- 1 Values provided for common rod material types based on published strengths and calculated in accordance with ACI 318 Eq. (D-3) and Eq. (D-20). Other material specifications are admissible, subject to the approval of the code official. Nuts and washers must be appropriate for the rod strength.
- 2 For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of f must be determined in accordance with ACI 318 D.4.5. Values correspond to a brittle steel element.

Table 18 — Concrete Breakout Design Information for Canadian Metric Reinforcing Bars¹

*

Design Information	Symbol	Units	Bar size			
Design information	Symbol	Units	10 M	15 M	20 M	25 M
Effectiveness factor for uncracked concrete	le.	SI	10	10	10	11.3
Ellectiveness factor for uncracked concrete	k _{c,uncr}	(in-lb)	(24)	(24)	(24)	(27)
Effectiveness factor for cracked concrete	le.	SI	7	7	7	7
Ellectiveness factor for cracked concrete	k _{c,cr}	(in-lb)	(17)	(17)	(17)	(17)
Minimum har angaing4	•	mm	57	80	98	126
Minimum bar spacing ⁴	S _{min}	(in.)	(2.2)	(3.1)	(3.8)	(5.0)
Minimum edge distance ⁴	C _{min}	mm	57	80	98	126
Willimum eage distance		(in.)	(2.2)	(3.1)	(3.8)	(5.0)
National was an expellent their land on a	_	mm	h _{ef} + 30	L 0.1 (2)		
Minimum member thickness	h _{min}	(in.)	(h _{ef} + 1-1/4)		$h_{ef} + 2d_0^{(3)}$	
Critical edge distance — splitting	_		0	0	10 of this document	
(for uncracked concrete)	C _{ac}	-	See Section 3.2.3.3.10 of this document.			۱۲.
Strength reduction factor for tension,	Φ.		0.05			
concrete failure modes, Condition B ²	Ф	-	0.65			
Strength reduction factor for shear,	Φ		0.70			
concrete failure modes, Condition B ²	Ψ	_		<u> </u>	70	

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

- $1 \ \ \text{For additional setting information, see installation instructions in Figure 5}.$
- 2 Values provided for post-installed anchors with category as determined from ACI 355.2 given for Condition B. Condition B applies without supplementary reinforcement or where pullout (bond) or pryout govern, as set forth in ACI 318 D.4.4, while condition A requires supplemental reinforcement. Values are for use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of f must be determined in accordance with ACI 318 D.4.5.
- 3 d_o = drill bit diameter.
- 4 For installations with a 1-3/4 in. edge distance, the installation torque must be reduced. Please refer to section 3.2.3.3.9.



Table 19 — Bond Strength Design Information for Canadian Metric Reinforcing Bars¹

*

Design Information		Symbol	Units		Bar Size			
Desig			Symbol	Ullits	10 M	15 M	20 M	25 M
		Characteristic bond strength	_	MPa		8	.9	
	A	in uncracked concrete	τ _{k,uncr}	(psi)		(1,2	290)	
	^	Characteristic bond strength	_	MPa	4.9	5.7	6.0	6.2
Je ²		in cracked concrete ³	$ au_{k,cr}$	(psi)	(705)	(822)	(884)	(895)
anç		Characteristic bond strength	_	MPa		7	.2	
Temperature range ²	B	in uncracked concrete	$ au_{ ext{k,uncr}}$	(psi)		(1,0	045)	
		Characteristic bond strength	_	MPa	3.9	4.6	4.9	5.0
Jωbe		in cracked concrete ³	$ au_{k,cr}$	(psi)	(569)	(663)	(712)	(722)
<u> </u>		Characteristic bond strength	τ _{k,uncr}	MPa	4.2			
	C	in uncracked concrete		(psi)	(605)			
		Characteristic bond strength	_	MPa	2.2	2.6	2.8	2.9
		in cracked concrete ³	$ au_{k,cr}$	(psi)	(326)	(379)	(408)	(412)
Minim	num a	nchor embedment depth	h	mm	60	80	90	101
			h _{ef,min}	(in.)	(2.4)	(3.1)	(3.5)	(4.0)
Maxin	num a	anchor embedment depth	h	mm	226	320	390	504
			h _{ef,max}	(in.)	(8.9)	(12.6)	(15.4)	(19.8)
<u>σ</u> ς <u>α</u>		Anchor						
Ssib	tion	Day and Water ast water a second	Category	-			I	
Permissible installation	conditions	Dry concrete and Water-saturated concrete	Ф _d & Ф _{ws}	=	0.65			

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

- 1 Bond strength values correspond to concrete compressive strength range 2,500 psi $\leq f' \leq 4,500$ psi. For 4,500 psi $\leq f' \leq 6,500$ psi, tabulated characteristic bond strengths may be increased by 6 percent. For 6,500 psi $\leq f' \leq 8,000$ psi, tabulated characteristic bond strengths may be increased by 10 percent.
- 2 Temperature range A: Maximum short term temperature = 104°F (40°C), maximum long term temperature = 75°F (24°C). Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C). Temperature range C: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 162°F (72°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

3 For structures assigned to Seismic Design Categories C, D, E or F, bond strength values are multiplied by a_{N,seis} = 1.0 => no reduction.



Resistance of HIT-HY 150 MAX-SD to Chemicals

Chemical		Behavior
Sulphuric acid	conc.	_
	30%	_
	10%	+
Hydrochloric acid	conc.	•
	10%	+
Nitric acid	conc.	_
	10%	•
Acetic acid	conc.	•
	10%	+
Formic acid	conc.	_
	10%	•
Lactic acid	conc.	+
	10%	+
Citric acid	10%	+
Sodium Hydroxide	40%	•
(Caustic soda)	20%	+
ĺ	5%	+
Ammonia	conc.	•
	5%	+
Soda solution	10%	+
Common salt solution	10%	+
Chlorinated lime solution	10%	+
Sodium hypochlorite	2%	+
Hydrogen peroxide	10%	+
Carbolic acid solution	10%	_
Ethanol		_
Sea water		+
Glycol		+
Acetone		-
Carbon tetrachloride		_
Toluene		+
Petrol/Gasoline		•
Machine oil		•
Diesel oil		•

Key: - non-resistant + resistant • limited resistance

5

3.2.3.5 Installation Instructions

Adhesive anchoring system for fastenings in concrete

Prior to use of product, follow instructions for use and recommended safety precautions. Check expiration date: See expiration date imprint on foilpack manifold. (Month/Year). Do not use an expired product.

Foil pack temperature: Must be between 32 °F and 104 °F (0 °C and 40 °C) when in use.

Base material temperature at time of installation: Must be between 14 $^{\circ}$ F and 104 $^{\circ}$ F (-10 $^{\circ}$ C and 40 $^{\circ}$ C).

Instructions for transport and storage: Keep in a cool, dry and dark place between 41 $^{\circ}$ F to 77 $^{\circ}$ F (5 $^{\circ}$ C to 25 $^{\circ}$ C).

Material Safety Data Sheet: Review the MSDS before use.

Installation instructions: Follow the illustrations for the sequence of operations and refer to tables for setting details. For any application not covered by this document, contact Hilti.

- **Drill hole** to the required depth h_o with a hammer-drill set in rotation hammer mode using an appropriately sized carbide drill bit. For holes drilled with other drill types contact a Hilti representative.
- Clean hole: Cleaning method has to be decided based on borehole condition. Just before setting an anchor/rebar, the borehole must be free of dust, water and debris by one of the following methods:

Method 1 — for dry or water saturated concrete (refer to pictograms): Compressed air cleaning is permissible for all diameters and embedment depths.

- Blow from the back of the borehole with oil-free compressed air (min. 90psi at 3.5 CFM (6 bar at 6 m³/h)) fully retracting the air extension 2 times until return air stream is free of noticeable dust.
- Brush 2 times with the specified Hilti HIT-RB brush size (brush φ ≥ bore hole φ) by inserting the round steel brush to the back of the borehole in a twisting motion and removing it. The brush should resist insertion into the borehole if not, the brush is too small and must be replaced with a brush of appropriate brush diameter.
- Blow again with compressed air 2 times until return air stream is free of noticeable dust.

If required use extensions for air nozzle and brushes to reach back of deep hole.

Method 2 — for standing water (e.g. water flows into cleaned borehole):

- Flush hole 2 times by inserting a water hose (water-line pressure) to the back of the borehole until water runs clear.
- Brush 2 times with the specified Hilti HIT-RB brush size (brush φ ≥ borehole φ) by inserting the round steel brush to the back of the borehole with a twisting motion and removing it. The brush should resist insertion into the borehole — if not, the brush is too small and must be replaced with a brush of appropriate brush diameter.
- Flush again 2 times until water runs clear. Remove all standing water completely (i.e. vacuum, compressed air or other appropriate procedure). To attain a dried borehole, a Hilti HIT-DL air nozzle attachment is

- recommended for borehole depth ≤ 10 inch (250 mm) and required for borehole depth > 10 inch (250 mm).
- Continue with borehole cleaning as described in Method 1.
- Insert foil pack in foil pack holder. Never use damaged foil packs and/or damaged or unclean foil pack holders.

 Attach new mixer prior to dispensing a new foil pack (snug fit)
- Tightly attach Hilti HIT-RE-M mixer to foil pack manifold. Do not modify the mixer in any way. Make sure the mixing element is in the mixer. Use only the mixer supplied with the anchor adhesive.
- Insert foil pack holder with foil pack into HIT-dispenser.

 Push release trigger, retract plunger and insert foil pack holder into the appropriate Hilti dispenser.
- Discard initial anchor adhesive. The foil pack opens automatically as dispensing is initiated. Do not pierce the foilpack manually (can cause system failure). Depending on the size of the foil pack an initial amount of anchor adhesive has to be discarded. See pictogram 8 for discard quantities. Dispose discarded anchor adhesive into the empty outer packaging. If a new mixer is installed onto a previously-opened foil pack, the first trigger pulls must also be discarded as described above. For each new foil pack a new mixer must be used.
- Inject anchor adhesive from the back of the borehole without forming air voids:
 - Injection method for borehole with depth 10 inch/250 mm:
 - Inject the anchor adhesive starting at the back of the hole (use the extension for deep holes), slowly withdraw the mixer with each trigger pull. Fill holes approximately 2/3 full, or as required to ensure that the annular gap between the anchor/rebar and the concrete is completely filled with anchor adhesive along the embedment length. After injection is completed, depressurize the dispenser by pressing the release trigger. This will prevent further anchor adhesive discharge from the mixer.
 - Piston plug injection is recommended for borehole depth > 10 inch/250 mm. The installation overhead is only possible with the aid of piston plugs. Assemble HIT-RE-M mixer, extension(s) and appropriately sized piston plug. Insert piston plug HIT-SZ/IP to back of the hole, and inject anchor adhesive as described in the injection method above. During injection the piston plug will be naturally extruded out of the bore hole by the anchor adhesive pressure. (HIT-SZ (IP) is not available or required for 7/16" diameter drilled hole.)
 - Insert anchor/rebar into bore hole. Mark and set anchor/ rebar to the required embedment depth. Before use, verify that the anchor/rebar is dry and free of oil and other contaminants. To ease installation, anchor/rebar may be slowly twisted as they are inserted. Use only Hilti anchor rods or equivalent. After installing an anchor/ rebar, the annular gap must be completely filled with anchor adhesive.

Attention! For overhead applications take special care when inserting the anchor/ rebar. Excess adhesive will be forced out of the borehole — take appropriate steps to prevent it from falling onto the installer. Position the anchor/ rebar and secure it from moving/falling during the curing time (e.g. wedges).

12

- Observe the gel time "t_{gel}", which varies according to temperature of base material. Minor adjustments to the anchor/rebar position may be performed during the gel time. See table 12. Once the gel time has elapsed, do not disturb the anchor/rebar until the curing time "t...." has elapsed.
- the anchor/rebar until the curing time " t_{cure} " has elapsed.

 Apply designed load/torque after " t_{cure} " has passed, and the fixture to be attached has been positioned. See table 13.

Partly used foil packs must be used up within four weeks. Leave the mixer attached on the foil pack manifold and store under the recommended storage conditions. If reused, attach a new mixer and discard the initial quantity of anchor adhesive as described by point 8

Safety instructions:

For industrial use only. Keep out of the reach of children. See the Material Safety Data Sheet for this product before handling.

Caution: Irritating to eyes and skin. May cause sensitization in susceptible individuals.

Contains: dibenzoyl peroxide.

Precautions: Avoid contact with skin/eyes. Always wear impermeable gloves and eye protection when using product. Store in a

cool, dry area. Keep from freezing. Do not store in direct sunlight.

First Aid: Eyes — Immediately flush with water for 15 minutes, contact a physician. Skin — Wash with soap and water. launder contaminated clothing before reuse. If irritations occurs, contact physician. Ingestion — Do not induce vomiting unless directed by a physician. Contact a physician immediately. Inhalation — Move to fresh air, give oxygen if breathing is difficult. contact a physician if symptoms persist.

Ingredient	CAS Number	Ingredient	CAS Number
Part A: (Large side)		Part B: (Small side)	
NJ Trade Secret Registry	19136100-5001	Quartz Sand	14808-60-7
Quartz Sand	14808-60-7	Water	07732-18-5
NJ Trade Secret Registry	19136100-5003	Dibenzoyl peroxide	00094-36-0
NJ Trade Secret Registry	19136100-5004	Aluminum oxide	01344-28-1
NJ Trade Secret Registry	19136100-5005	Amorphous silica	07631-86-9
Amorphous silica	67762-90-7	1,2,3-Propantriol	00056-81-5
NJ Trade Secret Registry	19136100-5002		
NJ Trade Secret Registry	19136100-5017		
NJ Trade Secret Registry	19136100-5019		

* NJ TSNR = New Jersey Trade Secret Registry Number

In Case of Emergency, call Chem-Trec: 1-800-424-9300 (USA, P.R., Virgin Islands, Canada)

En cas d'urgence, téléphoner Chem-Trec: 1-800-424-9300 (USA, P.R., Virgin Islands, Canada)

En Caso de Emergencia, llame Chem-Trec: 001-703-527-3887 (other countries/autres pays/otros países)

Made in Germany

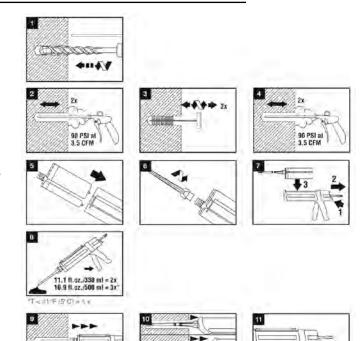
Net contents: 11.1 fl. oz (330 ml)/16.9 fl. oz (500 ml)

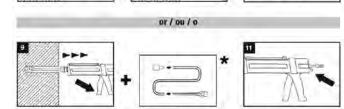
Net weight: 20.3 oz (575 g)/31.0 oz (880 g)

Warranty: Refer to standard Hilti terms and conditions of sale for

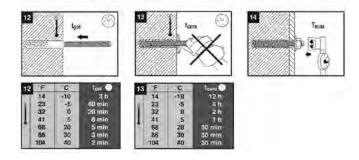
warranty information.

Failure to observe these installation instructions, use of non-Hilti anchors, poor or questionable concrete conditions, or unique applications may affect the reliability or performance of the fastenings. For full set of installation instructions see literature supplied with product packaging.





- Please refer to technical literature (approvals, setting instructions) for détail
 Voir littérature technique (agréments, manuels d'utilisation produits) pour plus de détail
- *) Por favor vease la referencia técnica (normativa y manuales de uso) para mas detalle



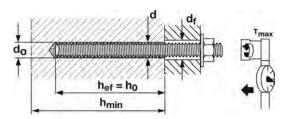


	HAS	Rebar	HIT-RB	HIT-SZ (IP)	HIT-DL
	Î		***************************************	В	
Ø [mm]	Ø [mm]	Ø [mm]	HIT-RB	HIT-SZ	HIT-DL
12	10	8	12	12	12
14	12	10	14	14	14
16	16	12	16	16	16
18	-	14	18	18	18
20	-	16	20	20	20
22	20	18	22	22	-
24	24	-	24	24	-
25	-	20	25	25	25
28	-	22	28	28	-
32	-	25	32	32	32

Ø [in.]	Ø [in.]	Size	HIT-RB	HIT-IP	HIT-DL
7/16	3/8	-	7/16"	-	-
1/2	-	#3	1/2"	1/2"	1/2"
9/16	1/2	10M	9/16"	9/16"	9/16"
5/8	-	#4	5/8"	5/8"	-
3/4	5/8	#5 & 15M	3/4"	3/4"	3/4"
7/8	3/4	#6	7/8"	7/8"	7/8"
1	7/8	#7 & 20M	1"	1"	1"
1-1/8	1	#8	1-1/8"	1-1/8"	-
1-1/4	-	25M	1-1/4"	1-1/4"	-

Drill bits must conform to tolerances in ANSI B212-1994. Les mèches de forage doivent être conformes à ANSI B212-1994. Brocas deben cumplir con el estándar ANSI B212-1994.

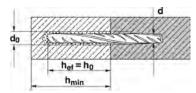
Setting Details of Hilti HIT-HY 150 MAX-SD with Threaded Rod



d	d_0	h _{ef} min-max	T _{max} *	d _f	h _{min}
[inch]	[inch]	[inch]	[ft-lb]	[inch]	[inch]
3/8	7/16	2-3/8 to 7-1/2	15	7/16	b +11/4
1/2	9/16	2-3/4 to 10	30	9/16	h _{ef} + 1-1/4
5/8	3/4	3-1/8 to 12-1/2	60	11/16	
3/4	7/8	3-1/2 to 15	100	13/16	h 10d
7/8	1	3-1/2 to 17-1/2	125	15/16	$h_{ef} + 2d_0$
1	1-1/8	4 to 20	150	1-1/8	

	[mm]	[mm]	[mm]	[Nm]	[mm]	[mm]
	M10	12	60 to 200	20	12	b ±30
	M12	14	70 to 240	40	14	h _{ef} + 30
	M18	18	80 to 320	80	18	
	M20	24	90 to 400	150	22	$h_{ef} + 2d_{0}$
١	M24	28	96 to 480	200	28	

Setting Details of Hilti HIT-HY 150 MAX-SD with Reinforcement Bars



d	d _o	h _{ef} min-max	h _{min}
US rebar	[inch]	[inch]	[inch]
#3	7/16	2-3/8 to 7-1/2	h _{ef} + 1-1/4
#4	5/8	2-3/4 to 10	
#5	3/4	3-1/8 to 12-1/2	
#6	7/8	3-1/2 to 15	h _{ef} + 2d ₀
#7	1	3-1/2 to 17-1/2	
#8	1-1/8	4 to 20	

Rebar [mm]	[mm]	[mm]	[mm]
10	14	60 to 200	h _{ef} + 30
12	16	70 to 240	
14	18	75 to 280	
16	20	80 to 320	h _{ef} + 2d ₀
20	25	90 to 400	
25	32	100 to 500	

CA rebar	[inch]	[inch]	[inch]
10 M	9/16	2-3/4 to 8-7/8	h _{ef} + 1-1/4
15 M	3/4	3-1/8 to12-1/2	
20 M	1	3-1/2 to 15-3/8	h _{ef} + 2d ₀
25 M	1-1/4	4 to 19-7/8	

* T_{max} : Edge Distance c_{ai} < (5 x d)				
Edge Distance c _{ai}	Anchor Spacing s _{min}	Maximum Torque		
1.75 in. (45 mm) ≤ c _{ai} < 5 x d	5 x d ≤ s _{min} < 16 in. (406 mm)	0.3 x T _{max}		
	s _{min} ≥ 16 in. (406 mm)	0.5 x T _{max}		

3.2.3.6 Ordering Information

HIT-HY 150 MAX-SD Fast Cure Hybrid Adhesive



Gel/Full Cure Time Table (Approximate)

том и том			
Material Tempe	erature		
°F	°C	t _{gel}	t _{cure}
14	-10	180 min	12 hrs
23	-5	40 min	4 hrs
32	0	20 min	2 hrs
50	10	8 min	1 hrs
68	20	5 min	30 min
86	30	3 min	30 min
104	40	2 min	30 min

Features and Applications

- First fast-cure adhesive anchor to comply with the latest building code, offering designers a strength design solution for anchors and rebar
- Fast cure time of approximately 30 min @ 68° F (20° C)
- Cold weather installation, 14° F base material temperature
- All seismic design categories and cracked concrete approval for maximum versatility

2003 IBC Compliant Anchor

2006 IBC Compliant Anchor

2009 IBC Compliant Anchor









Technical Data	HIT-HY 150 MAX-SD
Product	Hybrid Urethane Methacrylate
Base material temperature	14°F to 104°F (-10°C to 40°C)
Diameter range	3/8" to 1"

Listings/Approvals

- ICC-ES (International Code Council) -ESR-3013
- NSF/ANSI standard 61 -Certification for potable water
- COLA (City of Los Angeles) Research Report 25581

Package volume

- Volume of HIT 11.1 fl oz/330 ml foil pack is 20.1 in³
- Volume of HIT 16.9 fl oz/500 ml foil pack is 30.5 in³
- Volume of HIT 47.3 fl oz/1400 ml Jumbo foil pack is 85.4 in³



Order Information

Description	Package Contents	Qty
HIT-HY 150 MAX-SD (11.1 fl oz/330 mL) MC (1)	Includes (1) master carton containing 25 foil packs with (1) mixer and 3/8" filler tube per pack	25
HIT-HY 150 MAX-SD (11.1 fl oz/330 mL) MC (1) + MD 2500 Manual Dispenser	Includes (1) master carton containing 25 foil packs with 1 mixer and 3/8" filler tube per pack and (1) MD 2500 Manual Dispenser	25
HIT-HY 150 MAX-SD (16.9 fl oz/500 mL) MC (1) + MD 2500 Manual Dispenser	Includes (1) master carton containing 20 foil packs with 1 mixer and 3/8" filler tube per pack and (1) MD 2500 Manual Dispenser	20
HIT-HY 150 MAX-SD (16.9 fl oz/500 mL) MC (2) + MD 2500 Manual Dispenser	Includes (2) master cartons containing 20 foil packs each with 1 mixer and 3/8" filler tube per pack and (1) MD 2500 Manual Dispenser	40
HIT-HY 150 MAX-SD (16.9 fl oz/500 mL) MC (2) + ED 3500-A CPC Cordless Dispenser Kit	Includes (2) master cartons containing 20 foil packs each with 1 mixer and 3/8" filler tube per pack, (1) ED 3500-A CPC Cordless Dispenser, (2) B 144 2.6-Ah Li-Ion batteries and (1) C 4/36 Li-Ion charger	40
HIT-HY 150 MAX-SD (16.9 fl oz/500 mL) MC (5) + MD 2500 Manual Dispensers (2)	Includes (5) master cartons containing 20 foil packs each with 1 mixer and 3/8" filler tube per pack and (2) MD 2500 Manual Dispensers	100
HIT-HY 150 MAX-SD (16.9 fl oz/500 mL) MC (5) + ED 3500-A CPC Cordless Dispenser Kit	Includes (5) master cartons containing 20 foil packs each with 1 mixer and 3/8" filler tube per pack, (1) ED 3500-A CPC Cordless Dispenser, (2) B 144 2.6-Ah Li-Ion batteries and (1) C 4/36 Li-Ion charger	100
HIT-HY 150 MAX-SD (47.3 fl oz/1400 mL) MC (16) + P 8000 Pneumatic Dispenser (1) — 1 pallet	Includes (16) master cartons containing 4 jumbo foil packs each with 1 mixer and 3/8" filler tube per pack and (1) P 8000 Pneumatic Dispenser	64
HIT-HY 150 MAX-SD (47.3 fl oz/1400 mL) MC (32) + P 8000 Pneumatic Dispenser (1) — 2 pallets	Includes (32) master cartons containing 4 jumbo foil packs each with 1 mixer and 3/8" filler tube per pack and (1) P 8000 Pneumatic Dispenser	128
HIT-HY 150 MAX-SD (47.3 fl oz/1400 mL) MC (64) + P 8000 Pneumatic Dispenser (1) — 4 pallets	Includes (64) master cartons containing 4 jumbo foil packs each with 1 mixer and 3/8" filler tube per pack and (1) P 8000 Pneumatic Dispenser	256

Refer to Section 3.2.6.5 for ordering information of HAS threaded rods.



3.2.3 HIT-HY 150 MAX-SD Adhesive Anchoring System

Dispensers

Order Description	Qty
ED 3500-A CPC 2.6-Ah Kit Includes dispenser, (2) 2.6-Ah Li-Ion battery, C 7/24 standard charger and accessories in an impact-resistant plastic tool box	1
ED 3500-A Dispenser Includes dispenser only in cardboard box	1
Battery Pack B 144 2.6-Ah CPC CPC Li-lon 2.6-Ah battery for SFH 144-A, SF 144-A, SID 144-A, SIW 144-A, SFL 14 and ED 3500-A Dispenser	1
Battery Charger C 4/36 Li-Ion 115 V Use with all 14.4 - 36 volt Hilti CPC lithium ion batteries	1
MD 2500 Manual Dispenser with Foil Pack Holder For use with HIT 11.1 fl oz/330ml and 16.9oz/500ml foil pack	1
Foil Pack Holder Replacement holder for MD 2500 and ED 3500 dispensers	1
HIT-P 8000D Pneumatic Dispenser For use wth HIT 47.3 fl oz/1400 ml jumbo foil pack	1
Jumbo Foil Pack Holder Replacement holder for P 8000D dispenser	1

Accessory Selection Table

Select the correct installation accessory according to the hole diameter Round Brush

Hole Diameter ¹	Round Brush (for brushing holes)	Piston Plug (for helping prevent air voids when injecting adhesive)	Air nozzle (for blowing out holes)
	41111111111111111111111111111111111111		***************************************
Inch	Description	Description	Description
7/16	HIT-RB 7/16"	-	-
1/2	HIT-RB 1/2"	HIT-IP 1/2"	HIT-DL 1/2"
9/16	HIT-RB 9/16"	HIT-IP 9/16"	HIT-DL 9/16"
5/8	HIT-RB 5/8"	HIT-IP 5/8"	
11/16	HIT-RB 11/16"	HIT-IP 11/16"	HIT-DL 11/16"
3/4	HIT-RB 3/4"	HIT-IP 3/4"	HIT-DL 3/4"
7/8	HIT-RB 7/8"	HIT-IP 7/8"	HIT-DL 7/8"
1	HIT-RB 1"	HIT-IP 1"	HIT-DL 1"
1-1/8	HIT-RB 1 1/8"	HIT-IP 1 1/8"	-
1-1/4	HIT-RB 1 1/4"	HIT-IP 1 1/4"	-
1- 3/8	HIT-RB 1 3/8"	HIT-IP 1 3/8"	HIT-DL 1 3/8"
1-1/2	HIT-RB 1 1/2"	HIT-IP 1 1/2"	•
1-3/4	HIT-RB 1 3/4"	HIT-IP 1 3/4"	-

¹ Refer to adhesive anchor system installation instructions to determine the proper hole diameter for the fastening element to be used



ICC-ES Evaluation Report

ESR-3013

Reissued April 1, 2011

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DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

REPORT HOLDER:

HILTI, INC. 5400 SOUTH 122ND EAST AVENUE TULSA, OKLAHOMA 74146 (800) 879-8000 www.us.hilti.com HiltiTechEng@us.hilti.com

EVALUATION SUBJECT:

HILTI HIT-HY 150 MAX-SD ADHESIVE ANCHORING SYSTEM FOR CRACKED AND UNCRACKED CONCRETE

1.0 EVALUATION SCOPE

Compliance with the following codes:

- 2009 International Building Code® (2009 IBC)
- 2009 International Residential Code® (2009 IRC)
- 2006 International Building Code® (2006 IBC)
- 2006 International Residential Code® (2006 IRC)
- 2003 International Building Code® (2003 IBC)
- 2003 International Residential Code® (2003 IRC)
- 2000 International Building Code® (2000 IBC)
- 2000 International Residential Code® (2000 IRC)

Property evaluated:

Structural

2.0 **USES**

The Hilti HIT-HY 150 MAX-SD Adhesive Anchoring System is used to resist static, wind, or earthquake (Seismic Design Categories A through F) tension and shear loads in cracked or uncracked normal-weight concrete having a specified compressive strength, f'_c , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa). The anchor system is an alternative to anchors described in Sections 1911 and 1912 of the 2009 and 2006 IBC and Sections 1912 and 1913 of the 2003 and 2000 IBC. The anchor systems may also be used where an engineered design is submitted in accordance with Section R301.1.3 of the 2009, 2006 and 2003 IRC, or Section R301.1.2 of the 2000 IRC.

3.0 DESCRIPTION

3.1 General:

The Hilti HIT-HY 150 MAX-SD Adhesive Anchoring System is comprised of the following components:

- Hilti HIT-HY 150 MAX-SD adhesive, packaged in foil packs.
- Adhesive mixing and dispensing equipment.
- Hole cleaning equipment.

The Hilti HIT-HY 150 MAX-SD Adhesive Anchoring System may be used with continuously threaded steel rods, or deformed steel reinforcing bars. The primary components of the Hilti Adhesive Anchoring System are shown in Figure 3 of this report.

Installation information and parameters, as included with each adhesive unit package, are shown in Figure 5 of this report.

3.2 Materials:

3.2.1 Hilti HIT-HY 150 MAX-SD Adhesive: Hilti HIT-HY 150 MAX-SD Adhesive is an injectable hybrid adhesive combining urethane methacrylate resin, hardener, cement and water. The resin and cement are kept separate from the hardener and water by means of a dual-cylinder foil pack attached to a manifold. The two components combine and react when dispensed through a static mixing nozzle attached to the manifold. Hilti HIT-HY 150 MAX-SD is available in 11.1-ounce (330 ml), 16.9-ounce (500 ml), and 47.3-ounce (1400 ml) foil packs. The manifold attached to each foil pack is stamped with the adhesive expiration date. The shelf life, as indicated by the expiration date, applies to unopened foil packs that are stored in accordance with the Instructions for Use, as illustrated in Figure 5 of this report.

- **3.2.2 Hole Cleaning Equipment:** Hole cleaning equipment, comprised of steel wire brushes and air nozzles, is described in Figure 5 of this report.
- **3.2.3 Dispensers:** Hilti HIT-HY 150 MAX-SD must be dispensed with manual dispensers, pneumatic dispensers, or electric dispensers provided by Hilti.

3.2.4 Anchor Elements:

3.2.4.1 Threaded Steel Rods: The threaded steel rods must be clean, continuously threaded rods (all-thread) in diameters as described in Tables 2 and 3 of this report. Steel design information for common grades of threaded rod and associated nuts are provided in Tables 5 and 8 of this report, and instructions for use are shown in Figure 5. Carbon steel threaded rods must be furnished with a 0.0002-inch-thick (0.005 mm) zinc electroplated coating in accordance with ASTM B 633 SC 1; or must be hot-dipped galvanized in accordance with ASTM A 153, Class C or D. Threaded rods must be straight and free of indentations or other defects along their length. The ends may be stamped with identifying marks and the embedded end may be blunt cut or cut on the bias (chisel point).

ICC ANSI

ICC-ES Evaluation Reports are not to be construed as representing aesthetics or any other attributes not specifically addressed, nor are they to be construed as an endorsement of the subject of the report or a recommendation for its use. There is no warranty by ICC Evaluation Service, LLC, express or implied, as to any finding or other matter in this report, or as to any product covered by the report.

3.2.4.3 Ductility: In accordance with ACI 318 Appendix D, in order for a steel element to be considered ductile, the tested elongation must be at least 14 percent and reduction of area must be at least 30 percent. Steel elements with a tested elongation of less than 14 percent or a reduction of area of less than 30 percent, or both, are considered brittle. Values for various steel materials are provided in Tables 2 through 4 of this report. Where values are nonconforming or unstated, the steel must be considered brittle.

3.3 Concrete:

Normal-weight concrete must comply with Sections 1903 and 1905 of the IBC. The specified compressive strength of the concrete must be from 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).

4.0 DESIGN AND INSTALLATION

4.1 Strength Design:

4.1.1 General: The design strength of anchors under the 2006 IBC and 2006 IRC must be determined in accordance with ACI 318-05 Appendix D and this report.

The design strength of anchors under the 2009, 2003, and 2000 IBC as well as Section 301.1.2 of the 2000 IRC and Section 301.1.3 of the 2009 and 2003 IRC, must be determined in accordance with ACI 318-08 Appendix D and this report.

A design example according to the 2006 IBC is given in Figure 4 of this report.

Design parameters are based on the 2009 IBC (ACI 318-08) unless noted otherwise in Section 4.1.1 through 4.1.12 of this report.

The strength design of anchors must comply with ACI 318 D.4.1, except as required in ACI 318 D.3.3.

Design parameters are provided in Tables 5 through Table 19. Strength reduction factors, ϕ , as given in ACI 318 D.4.4 must be used for load combinations calculated in accordance with Section 1605.2.1 of the IBC or Section 9.2 of ACI 318. Strength reduction factors, ϕ , as given in ACI 318 D.4.5 must be used for load combinations calculated in accordance with ACI 318 Appendix C.

The following amendments to ACI 318 Appendix D must be used as required for the strength design of adhesive anchors. In conformance with ACI 318, all equations are expressed in inch-pound units.

Modify ACI 318 Section D.4.1.2 as follows:

D.4.1.2—In Eq. (D-1) and (D-2), ϕN_n and ϕV_n are the lowest design strengths determined from all appropriate failure modes. ϕN_n is the lowest design strength in tension of an anchor or group of anchors as determined from consideration of $\phi N_{\rm sa}$, either $\phi N_{\rm a}$ or $\phi N_{\rm ag}$ and either $\phi N_{\rm cb}$ or $\phi N_{\rm cbg}$. ϕV_n is the lowest design strength in shear of an

anchor or a group of anchors as determined from consideration of: ϕV_{sa} , either ϕV_{cb} or ϕV_{cbg} , and either ϕV_{cp} or ϕV_{cpg} . For adhesive anchors subjected to tension resulting from sustained loading, refer to D.4.1.4 for additional requirements.

Add ACI 318 Section D.4.1.4 as follows:

D.4.1.4—For adhesive anchors subjected to tension resulting from sustained loading, a supplementary check shall be performed using Eq. (D-1), whereby N_{ua} is determined from the sustained load alone, e.g., the dead load and that portion of the live load acting that may be considered as sustained and ϕN_n is determined as follows:

D.4.1.4.1—For single anchors, $\phi N_n = 0.75 \phi N_{a0}$

D.4.1.4.2—For anchor groups, Eq. (D-1) shall be satisfied by taking $\phi N_n = 0.75 \phi N_{a0}$ for that anchor in an anchor group that resists the highest tension load.

D.4.1.4.3—Where shear loads act concurrently with the sustained tension load, the interaction of tension and shear shall be analyzed in accordance with D.4.1.3.

Modify ACI 318 D.4.2.2 in accordance with 2009 IBC section 1908.1.10 as follows:

D.4.2.2 – The concrete breakout strength requirements for anchors in tension shall be considered satisfied by the design procedure of D.5.2 provided Equation D-8 is not used for anchor embedments exceeding 25 inches. The concrete breakout strength requirements for anchors in shear with diameters not exceeding 2 inches shall be considered satisfied by the design procedure of D.6.2. For anchors in shear with diameters exceeding 2 inches, shear anchor reinforcement shall be provided in accordance with the procedures of D.6.2.9.

4.1.2 Static Steel Strength in Tension: The nominal static steel strength of a single anchor in tension, N_{sa} , in accordance with ACI 318 D.5.1.2 and strength reduction factor, ϕ , in accordance with ACI D.4.4 are given in the tables outlined in Table 1a for the corresponding anchor steel

4.1.3 Static Concrete Breakout Strength in Tension: The nominal static concrete breakout strength of a single anchor or group of anchors in tension, N_{cb} or N_{cbg} , must be calculated in accordance with ACI 318 D.5.2 with the following addition:

D 5.2.10 (2009 IBC) or D 5.2.9 (2006 IBC) —The limiting concrete strength of adhesive anchors in tension shall be calculated in accordance with D.5.2.1 to D.5.2.9 under the 2009 IBC or D.5.2.1 to D.5.2.8 under the 2006 IBC where the value of $k_{\rm c}$ to be used in Eq. (D-7) shall be:

 $k_{c,cr}$ where analysis indicates cracking at service load levels in the anchor vicinity (cracked concrete). The values of $k_{c,cr}$ are given in the Tables 6, 9, 12, 15, and 18 of this report.

 $k_{c,uncr}$ where analysis indicates no cracking at service load levels in the anchor vicinity (uncracked concrete). The values of $k_{c,uncr}$ are given in the Tables 6, 9, 12, 15, and 18 of this report.

The basic concrete breakout strength of a single anchor in tension, N_b , must be calculated in accordance with ACI D.5.2.2 using the values of h_{ef} , $k_{c,cr}$, and $k_{c,uncr}$ as described in the tables of this report. The modification factor " λ " shall be taken as 1.0. Anchors shall not be installed in lightweight concrete. The value of f_c used for calculation must be limited to 8,000 psi (55 MPa) in accordance with ACI 318 D.3.5.

4.1.4 Static Pullout Strength in Tension: In lieu of determining the nominal static pullout strength in accordance with ACI 318 D.5.3, nominal bond strength in tension must be calculated in accordance with the following sections added to ACI 318:

D.5.3.7—The nominal bond strength of a single adhesive anchor, N_{a_g} or group of adhesive anchors, N_{ag} , in tension shall not exceed

(a) for a single anchor

$$N_a = \frac{A_{Na}}{A_{Na0}} \cdot \psi_{ed,Na} \cdot \psi_{p,Na} \cdot N_{a0}$$
 (D-16a)

(b) for a group of anchors

$$N_{ag} = \frac{A_{Na}}{A_{Na0}} \cdot \psi_{ed,Na} \cdot \psi_{g,Na} \cdot \psi_{ec,Na} \cdot \psi_{p,Na} \cdot N_{a0}$$
 (D-16b)

where

 A_{Na} is the projected area of the failure surface for the single anchor or group of anchors that shall be approximated as the base of the rectilinear geometrical figure that results from projecting the failure surface outward a distance, $c_{cr,Na}$, from the centerline of the anchor, or in the case of a group of anchors, from a line through a row of adjacent anchors. A_{Na} shall not exceed nA_{Na0} where n is the number of anchors in tension in the group. In ACI 318 Figures RD.5.2.1a and RD.5.2.1b, the terms $1.5h_{ef}$ and $3.0h_{ef}$ shall be replaced with $c_{cr,Na}$ and $s_{cr,Na}$ respectively.

 A_{Na0} is the projected area of the failure surface of a single anchor without the influence of proximate edges in accordance with Eq. (D-16c):

$$A_{Na0} = \left(s_{cr,Na}\right)^2 \tag{D-16c}$$

with

 $s_{cr,Na}$ = as given by Eq. (D-16d).

D.5.3.8—The critical spacing $s_{cr,Na}$ and critical edge distance $c_{cr,Na}$ shall be calculated as follows:

$$s_{cr,Na} = 20 \cdot d \cdot \sqrt{\frac{\tau_{k,uncr}}{1,450}} \le 3h_{ef}$$
 (D-16d)

$$c_{cr,Na} = \frac{S_{cr,Na}}{2} \tag{D-16e}$$

D.5.3.9—The basic strength of a single adhesive anchor in tension in cracked concrete shall not exceed:

$$N_{a0} = \tau_{k,cr} \cdot \pi \cdot d \cdot h_{ef} \tag{D-16f}$$

where:

 $\tau_{k,cr}$ is the bond strength in cracked concrete

D.5.3.10—The modification factor for the influence of the failure surface of a group of adhesive anchors is:

$$\psi_{g,Na} = \psi_{g,Na0} + \left[\left(\frac{s}{s_{cr,Na}} \right)^{0.5} \cdot \left(1 - \psi_{g,Na0} \right) \right]$$
 (D-16g)

where

$$\psi_{g,Na0} = \sqrt{n} - \left[\left(\sqrt{n} - 1 \right) \cdot \left(\frac{\tau_{k,cr}}{\tau_{k,max,cr}} \right)^{1.5} \right] \ge 1.0 \tag{D-16h}$$

where

n = the number of tension-loaded adhesive anchors in a group.

$$\tau_{k,max,cr} = \frac{k_{c,cr}}{\pi \cdot d} \sqrt{h_{ef} \cdot f_c'}$$
 (D-16i)

The value of f'_c shall be limited to a maximum of 8,000 psi (55 MPa) in accordance with ACI 318 D.3.5.

D.5.3.11—The modification factor for eccentrically loaded adhesive anchor groups is:

$$\psi_{\text{ec,Na}} = \frac{1}{1 + \frac{2e'_N}{s_{\text{Cr Na}}}} \le 1.0 \tag{D-16j}$$

Eq. (D-16j) is valid for $e'_{N} = \frac{s}{2}$

If the loading on an anchor group is such that only certain anchors are in tension, only those anchors that are in tension shall be considered when determining the eccentricity e'_N for use in Eq. (D-16j).

In the case where eccentric loading exists about two orthogonal axes, the modification factor $\psi_{ec,Na}$ shall be computed for each axis individually and the product of these factors used as $\psi_{ec,Na}$ in Eq. (D-16b).

D.5.3.12—The modification factor for the edge effects for a single adhesive anchor or anchor groups loaded in tension is:

$$\psi_{ed,Na} = 1.0 \text{ when } c_{a,min} \ge c_{cr,Na}$$
 (D-16I)

OI

$$\psi_{ed,Na} = \left(0.7 + 0.3 \cdot \frac{c_{a,min}}{c_{cr,Na}}\right) \le 1.0 \text{ when } c_{amin} < c_{cr,Na}$$
 (D-16m)

D.5.3.13—When an adhesive anchor or a group of adhesive anchors is located in a region of a concrete member where analysis indicates no cracking at service load levels, the nominal strength, N_a or N_{ag} , of a single adhesive anchor or a group of adhesive anchors shall be calculated according to Eq. (D-16a) and Eq. (D-16b) with $T_{K,uncr}$ substituted for $T_{k,cr}$ in the calculation of the basic strength N_{ao} in accordance with Eq. (D-16f). The factor $\Psi_{g,Na0}$ shall be calculated in accordance with Eq. (D-16h) whereby the value of $T_{k,max,uncr}$ shall be calculated in accordance with Eq. (D-16h).

$$\tau_{k,max,uncr} = \frac{k_{c,uncr}}{\pi \cdot d} \sqrt{h_{ef} \cdot f'_{c}}$$
 (D-16n)

D.5.3.14—When an adhesive anchor or a group of adhesive anchors is located in a region of a concrete member where analysis indicates no cracking at service load levels, the modification factor $\psi_{p,Na}$ shall be taken as:

$$\psi_{p,Na} = 1.0 \text{ when } c_{a,min} \ge c_{ac}$$
 (D-16o)

$$\psi_{p,Na} = \frac{\max|c_{a,min;} c_{cr,Na}|}{c_{ac}} \text{ when } c_{a,min} < c_{ac}$$
 (D-16p)

where:

c_{ac} shall be determined in accordance with Section 4.1.10 of this report.

For all other cases: $\psi_{p,Na} = 1.0$ (e.g. when cracked concrete is considered).

Additional information for the determination of nominal bond strength in tension is given in Section 4.1.8 of this report.

4.1.5 Static Steel Strength in Shear: The nominal static steel strength of a single anchor in shear as governed by the steel, V_{sa} , in accordance with ACI 318 D.6.1.2 and strength reduction factor, ϕ , in accordance with ACI 318 D.4.4 are given in the tables outlined in Table 1a of this report for the corresponding anchor steel.

4.1.7 Static Concrete Pryout Strength in Shear: In lieu of determining the nominal static pryout strength in accordance with ACI 318 D.6.3.1, the nominal pryout strength in shear must be calculated in accordance with the following sections added to ACI 318:

D.6.3.2—The nominal pryout strength of an adhesive anchor or group of adhesive anchors shall not exceed:

(a) for a single adhesive anchor:

$$V_{cp} = min/k_{cp} \cdot N_a; k_{cp} \cdot N_{cb}$$
 (D-30a)

(b) for a group of adhesive anchors:

$$V_{cpg} = min/k_{cp} \cdot N_{ag}; k_{cp} \cdot N_{cbg} /$$
 (D-30b)

where

 $k_{cp} = 1.0 \text{ for } h_{ef} < 2.5 \text{ inches (64 mm)}$

 $k_{cp} = 2.0 \text{ for } h_{ef} \ge 2.5 \text{ inches (64 mm)}$

Na shall be calculated in accordance with Eq. (D-16a)

Nag shall be calculated in accordance with Eq. (D-16b)

 N_{cb} and N_{cbg} shall be determined in accordance with D.5.2.

4.1.8 Bond Strength Determination: Bond strength values are a function of the concrete compressive strength, whether the concrete is cracked or uncracked and the installation conditions (dry, water-saturated concrete). The resulting characteristic bond strength must be multiplied by the associated strength reduction factor ϕ_{nn} as follows:

CONCRETE TYPE	PERMISSIBLE INSTALLATION CONDITIONS	BOND STRENGTH	ASSOCIATED STRENGTH REDUCTION FACTOR
Uncracked	Dry	$ au_{k,uncr}$	$\phi_{ m d}$
Uncracked	Water-saturated	$ au_{k,uncr}$	$\phi_{ m ws}$
Cracked	Dry	$ au_{k,cr}$	Фа
Cracked	Water-saturated	T _{k,cr}	Øws

Figure 2 of this report presents a bond strength design selection flowchart. Strength reduction factors for determination of the bond strength are given in the tables outlined in Table 1a of this report. Adjustments to the bond strength may also be taken for increased concrete compressive strength. These factors are given in the corresponding tables as well.

4.1.9 Minimum Member Thickness, h_{min} , **Anchor spacing,** s_{min} , and **Edge Distance,** c_{min} : In lieu of ACI 318 D.8.3, values of c_{min} and s_{min} described in this report must be observed for anchor design and installation. In lieu of ACI 318 D.8.5, the minimum member thicknesses, h_{min} , described in this report must be observed for anchor

design and installation. In determining minimum edge distance, c_{min} , the following section must be added to ACI 318:

D.8.8—For adhesive anchors that will remain untorqued, the minimum edge distance shall be based on minimum cover requirements for reinforcement in 7.7. For adhesive anchors that will be torqued, the minimum edge distance and spacing are given in Tables 6, 9, 12, 15, and 18 of this report.

For edge distances c_{ai} and anchor spacing s_{ai} the maximum torque T'_{max} shall comply with the following requirements:

REDUCED INSTALLATION TORQUE T_{max} FOR EDGE DISTANCES c_{ai} < (5 x d)			
EDGE DISTANCE, cai MINIMUM ANCHOR SPACING, sai		=> MAXIMUM TORQUE, T _{max}	
1.75 in. (45 mm) ≤ c _{ai}	5 x d ≤ s _{ai} < 16 in.	0.3 x T _{max}	
< 5 x d	s _{ai} ≥ 16 in. (406 mm)	$0.5 \times T_{max}$	

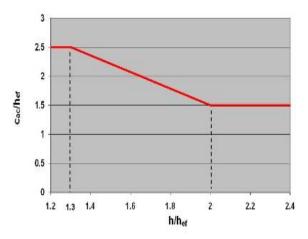
4.1.10 Critical Edge Distance, c_{ac}: For the calculation of N_{cb} , N_{cbg} , N_a and N_{ag} in accordance with ACI 318 Section D.5.2.7 and Section 4.1.4 of this report, the critical edge distance, c_{ac} , must be determined as follows:

i. $c_{ac} = 1.5 h_{ef}$ for $h/h_{ef} \ge 2$

ii. $c_{ac} = 2.5 h_{ef}$ for $h/h_{ef} \le 1.3$

For definitions of h and h_{ef} , see Figure 1 of this report.

For definitions of h and h_{ef} , see Figure 1 of this report.



Linear interpolation is permitted to determine the ratio c_{ac}/h_{ef} for values of h/h_{ef} between 2 and 1.3 as illustrated in the graph above.

4.1.11 Design Strength in Seismic Design Categories C, D, E and F: In structures assigned to Seismic Design Category C, D, E or F under the IBC or IRC, the design must be performed according to ACI 318 Section D.3.3, and the anchor strength must be adjusted in accordance with 2009 IBC Section 1908.1.9 or 2006 IBC Section 1908.1.16. For brittle steel elements, the anchor strength must be adjusted in accordance with ACI 318-05 D.3.3.5 or ACI 318-08 D.3.3.5 or D.3.3.6. The nominal steel shear strength, V_{sa} , must be adjusted by $\alpha_{V,seis}$ as given in the tables summarized in Table 1a for the corresponding anchor steel. An adjustment of the nominal bond strength $\tau_{k,cr}$ by $\alpha_{N,seis}$ is not necessary since $\alpha_{N,seis}$ = 1.0 in all cases.

4.1.12 Interaction of Tensile and Shear Forces: For designs that include combined tension and shear, the interaction of tension and shear loads must be calculated in accordance with ACI 318 D.7.

4.2 Allowable Stress Design:

4.2.1 General: For anchors designed using load combinations in accordance with IBC Section 1605.3 (Allowable Stress Design), allowable loads must be established using Eq. (4-1) or Eq. (4-2):

$$T_{allowable,ASD} = \frac{\phi N_n}{\alpha}$$
 Eq. (4-1)

and

$$V_{allowable,ASD} = \frac{\phi V_n}{\alpha}$$
 Eq. (4-2)

where

 $T_{allowable,ASD}$ = Allowable tension load (lbf or kN)

 $V_{allowable,ASD}$ = Allowable shear load (lbf or kN)

 ϕN_n = Lowest design strength of an anchor or anchor group in tension as determined in accordance with ACI 318 Appendix D with amendments in this report and 2009 IBC Sections 1908.1.9 and 1908.1.10 or 2006 IBC Section 1908.1.16, as applicable.

 ϕV_n = Lowest design strength of an anchor or anchor group in shear as determined in accordance with ACI 318 Appendix D with amendments in Section 3.3 of this criteria and 2009 IBC Sections 1908.1.9 and 1908.1.10 or 2006 IBC Section 1908.1.16, as applicable.

 α = Conversion factor calculated as a weighted average of the load factors for the controlling load combination. In addition, α must include all applicable factors to account for non-ductile failure modes and required over-strength.

Limits on edge distance, anchor spacing and member thickness described in this report must apply.

Example calculations for derivation of $T_{allowable,ASD}$ are provided in Table 1b.

4.2.2 Interaction of Tensile and Shear Forces: In lieu of ACI 318 D.7.1, D.7.2 and D.7.3, interaction must be calculated as follows:

For shear loads $V \le 0.2 \cdot V_{allow,ASD}$, the full allowable load in tension $T_{allow,ASD}$ may be taken.

For tension loads $T \le 0.2 \cdot T_{allow,ASD}$, the full allowable load in shear $V_{allow,ASD}$ may be taken.

For all other cases:

$$\frac{r}{T_{allowable,ASD}} + \frac{v}{V_{allowable,ASD}} \le 1.2$$
 Eq. (4-3)

4.3 Installation:

Installation parameters are illustrated in Figure 1 of this report. Anchor locations must comply with this report and the plans and specifications approved by the code official. Installation of the Hilti HIT-HY 150 MAX-SD Adhesive Anchor System must conform to the manufacturer's published installation instructions included in each unit package, as provided in Figure 5 of this report.

4.4 Special Inspection:

Periodic special inspection must be performed where required in accordance with Sections 1704.4 and 1704.15 of the 2009 IBC or Section 1704.13 of the 2006, 2003 and 2000 IBC, whereby periodic special inspection is defined in Section 1702.1 of the IBC and this report. The special inspector must be on the jobsite initially during anchor installation to verify anchor type, anchor dimensions,

concrete type, concrete compressive strength, hole dimensions, hole cleaning procedures, anchor spacing, edge distances, concrete thickness, anchor embedment, and tightening torque. The special inspector must verify the initial installations of each type and size of adhesive anchor by construction personnel on the site. Subsequent installations of the same anchor type and size by the same construction personnel are permitted to be performed in the absence of the special inspector. Any change in the anchor product being installed or the personnel performing the installation requires an initial inspection. For ongoing installations over an extended period, the special inspector must make regular inspections to confirm correct handling and installation of the product.

Continuous special inspection is required for all cases where anchors installed overhead (vertical up) are designed to resist sustained tension loads.

Under the IBC, additional requirements as set forth in Sections 1705, 1706 or 1707 must be observed, where applicable.

5.0 CONDITIONS OF USE

The Hilti HIT-HY 150 MAX-SD Adhesive Anchoring System described in this report complies with, or is a suitable alternative to what is specified in, those codes listed in Section 1.0 of this report, subject to the following conditions:

- 5.1 The Hilti HIT-HY 150 MAX-SD Adhesive Anchoring System must be installed in accordance with the manufacturer's published installation instructions, as included in the adhesive packaging and described in Figure 5 of this report.
- **5.2** The anchors must be installed in cracked or uncracked normal-weight concrete having a specified compressive strength f'_c = 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa).
- **5.3** The values of f'_c used for calculation purposes must not exceed 8,000 psi (55 MPa).
- 5.4 Anchors must be installed in concrete base materials in holes predrilled in accordance with the instructions provided in Figure 5 of this report.
- 5.5 Loads applied to the anchors must be adjusted in accordance with Section 1605.2 of the IBC for strength design and in accordance with Section 1605.3 of the IBC for allowable stress design.
- 5.6 Hilti HIT-HY 150 MAX-SD adhesive anchors are recognized for use to resist short- and long-term loads, including wind and earthquake, subject to the conditions of this report.
- 5.7 In structures assigned to Seismic Design Category C, D, E or F under the IBC or IRC, anchor strength must be adjusted in accordance with 2009 IBC Section 1908.1.9 or 2006 IBC Section 1908.1.16.
- 5.8 Hilti HIT-HY 150 MAX-SD adhesive anchors are permitted to be installed in concrete that is cracked or that may be expected to crack during the service life of the anchor, subject to the conditions of this report.
- **5.9** Strength design values must be established in accordance with Section 4.1 of this report.
- 5.10 Allowable stress design values must be established in accordance with Section 4.2 of this report.
- 5.11 Minimum anchor spacing and edge distance as well as minimum member thickness must comply with the values given in this report.

- 5.12 Prior to anchor installation, calculations and details demonstrating compliance with this report shall be submitted to the code official. The calculations and details must be prepared by a registered design professional where required by the statutes of the jurisdiction in which the project is to be constructed.
- 5.13 Anchors are not permitted to support fire-resistive construction. Where not otherwise prohibited by the code, the Hilti HIT-HY 150 MAX-SD Adhesive Anchoring System is permitted for installation in fireresistive construction provided that at least one of the following conditions is fulfilled:
 - Anchors are used to resist wind or seismic forces only.
 - Anchors that support gravity load—bearing structural elements are within a fire-resistive envelope or a fire-resistive membrane, are protected by approved fire-resistive materials, or have been evaluated for resistance to fire exposure in accordance with recognized standards.
 - Anchors are used to support nonstructural elements.
- 5.14 Since an ICC-ES acceptance criteria for evaluating data to determine the performance of adhesive anchors subjected to fatigue or shock loading is unavailable at this time, the use of these anchors under such conditions is beyond the scope of this report
- **5.15** Use of zinc-plated carbon steel threaded rods or steel reinforcing bars is limited to dry, interior locations.
- 5.16 Use of hot-dipped galvanized carbon steel and stainless steel rods is permitted for exterior exposure or damp environments.

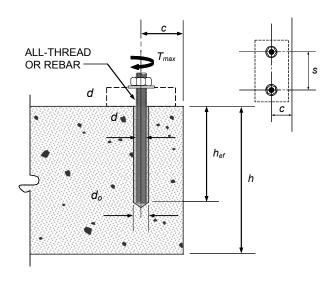
- 5.17 Steel anchoring materials in contact with preservative-treated and fire-retardant-treated wood must be of zinc-coated carbon steel or stainless steel. The minimum coating weights for zinc-coated steel must comply with ASTM A 153.
- 5.18 Periodic special inspection must be provided in accordance with Section 4.4 of this report. Continuous special inspection for overhead installations (vertical up) that are designed to resist sustained tension loads must be provided in accordance with Section 4.4 of this report.
- 5.19 Hilti HIT-HY 150 MAX-SD adhesive is manufactured by Hilti GmbH, Kaufering, Germany, with quality control inspections by Underwriters Laboratories Inc. (AA-668).

6.0 EVIDENCE SUBMITTED

Data in accordance with the ICC-ES Acceptance Criteria for Post-installed Adhesive Anchors in Concrete (AC308), dated November 2009, including but not limited to tests under freeze/thaw conditions (Table 4.2, test series 6).

7.0 IDENTIFICATION

- 7.1 The adhesives are identified by packaging labeled with the manufacturer's name (Hilti Corp.) and address, product name, a lot number, the expiration date, the evaluation report number (ICC-ES ESR-3013), and the name of the inspection agency (Underwriters Laboratories Inc).
- 7.2 Threaded rods, nuts, washers, and deformed reinforcing bars are standard elements and must conform to applicable national or international specifications as set forth in Tables 2, 3 and 4 of this report.



THREADED ROD / REINFORCING BAR FIGURE 1—INSTALLATION PARAMETERS

TABLE 1a—DESIGN TABLE INDEX

DESIGN STRENGTH ¹		THREADE	D ROD	DEFORMED REINFORCEMENT				
		Fractional	Metric	U.S. (imperial)	EU (metric)	Canadian (metric)		
Steel	Steel N_{sa} , V_{sa}		Table 8	Table 11	Table 14	Table 17		
Concrete	Concrete N_{cb} , N_{cbg} , V_{cb} , V_{cbg} , V_{cp} , V_{cpg}		Table 9	Table 12	Table 15	Table 18		
Bond ²			Table 10	Table 13	Table 16	Table 19		

¹Design strengths are as set forth in ACI 318 D.4.1.2. ² See Section 4.1 of this report for bond strength information.

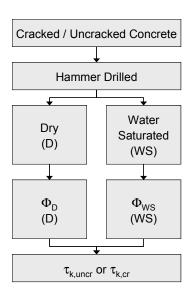


FIGURE 2—FLOWCHART FOR ESTABLISHMENT OF DESIGN BOND STRENGTH

TABLE 1b—EXAMPLE ALLOWABLE STRESS DESIGN VALUES FOR ILLUSTRATIVE PURPOSES

NOMINAL ANCHOR DIAMETER	EFFECTIVE EMBEDMENT DEPTH	f'c	k _{c,uncr}	α	φ	N _n	ALLOWABLE TENSION LOAD $\phi N_n / \alpha$	
d	h _{ef}						φ. τη, ω	
(in.)	(in.)	(psi)	(-)	(-)	(-)	(lb)	(lb)	
3/8	2 ³ / ₈	2,500	24	1.48	0.65	4,392	1,928	
1/2	2 ³ / ₄	2,500	24	1.48	0.65	5,472	2,403	
5/8	3 ¹ / ₈	2,500	24	1.48	0.65	6,629	2,911	
3/4	3 ¹ / ₂	2,500	24	1.48	0.65	7,857	3,450*	
⁷ / ₈	3 ¹ / ₂	2,500	27	1.48	0.65	8,839	3,882	
1	4	2,500	27	1.48	0.65	10,800	4,743	

For **SI**: 1 lb = 4.45 kN, 1 psi = 0.00689 MPa, 1 in. = 25.4 mm, $^{\circ}$ C = $[(^{\circ}F) - 32]/1.8$

Design Assumptions:

- 1. Single anchor with static tension load only; ASTM A 193 Grade B7 threaded rod, ductile.
- 2. Vertical downward installation direction.
- 3. Inspection Regimen = Periodic.
- 4. Installation temperature = 14 104 °F.
- 5. Long term temperature = 75 °F.
- 6. Short term temperature = 104 °F.
- 7. Dry hole condition carbide drilled hole.
- 8. Embedment depth = $h_{ef min}$.
- 9. Concrete determined to remain uncracked for the life of the anchorage.
- 10. Load combination from ACI 318 Section 9.2 (no seismic loading).
- 11. 30 percent Dead Load (D) and 70 percent Live Load (L); Controlling load combination 1.2 D + 1.6 L.
- 12. Calculation of α based on weighted average: $\alpha = 1.2 \, \text{D} + 1.6 \, \text{L} = 1.2 \, (0.30) + 1.6 \, (0.70) = 1.48$.
- 13. Normal weight concrete: $f_c = 2,500 \text{ psi}$
- 14. Edge distance: $c_{a1} = c_{a2} > c_{ac}$
- 15. Member thickness: $h \ge h_{min}$.

	* Verify capacity											
Capacity	ACI 318 reference	Formula	Calculation	φ	<i>ø</i> N _n							
Steel	D.5.1	$N_{sa} = nA_{se,N}f_{uta}$	$N_{sa} = 0.3345 \cdot 125,000$	0.75	31,360 lb							
Concrete	D.5.2	$N_{cb} = k_{c,uncr} (f'_c)^{0.5} h_{ef}^{1.5}$	$N_{cb} = 24 \cdot (2,500)^{0.5} \cdot 3.5^{1.5}$	0.65	5,107 lb							
Bond	D.5.3**	$N_a = \pi \square d h_{ef} \tau_{k uncr}$	$N_a = \pi \cdot 3/4 \cdot 3.5 \cdot 1,710$	0.65	9,166 lb							

 \rightarrow concrete breakout is decisive; hence the ASD value will be calculated as $\frac{5,107 \text{ lb}}{1.48}$ = 3,450 lb

** Design equation provided in Section 4.1.4 as new section ACI 318 D.5.3.9, Eq. (D-16f).

TABLE 2—TENSILE PROPERTIES OF COMMON CARBON STEEL THREADED ROD MATERIALS1

THREADED ROD SPECIFIC	THREADED ROD SPECIFICATION		MINIMUM SPECIFIED YIELD STRENGTH 0.2% OFFSET, f _{YA}	f _{UTA} f _{YA}	MINMUM ELONGATION, PERCENT ⁵	MINIMUM REDUCTION OF AREA, PERCENT	SPECIFICATION FOR NUTS ⁶	
ASTM A 193 ² Grade B7	psi	125,000	105,000	1.19	16	50	ASTM A194	
$\leq 2^{1}/_{2}$ in. (≤ 64 mm)	(MPa)	(860)	(725)	1.10	10	00		
ASTM F 568M³ Class 5.8	MPa	500	400				DIN 934 (8-A2K)	
M5 (¹ / ₄ in.) to M24 (1 in.) (equivalent to ISO 898-1)	(psi)	(72,500)	(58,000)	1.25	10	35	ASTM A563 Grade DH ⁷	
	MPa	500	400					
ISO 898-1 ⁴ Class 5.8	(psi)	(72,500)	(58,000)	1.25	22	-	DIN 934 (Grade 6)	
ISO 898-1 ⁴ Class 8.8	MPa	800	640	1.25	12	52	DIN 934 (Grade 8)	
130 030-1 Class 0.0	(psi)	(116,000)	(92,800)	1.25	12	52	Dily 334 (Glade 6)	

¹ Hilti HIT-HY 150 MAX-SD adhesive may be used in conjunction with all grades of continuously threaded carbon steel rod (all-thread) that comply with the code reference standards and that have thread characteristics comparable with ANSI B1.1 UNC Coarse Thread Series or ANSI B1.13M M Profile Metric Thread Series. Values for threaded rod types and associated nuts supplied by Hilti are provided here.

TABLE 3—TENSILE PROPERTIES OF COMMON STAINLESS STEEL THREADED ROD MATERIALS1

THREADED ROD SPECIFICATION		MINIMUM SPECIFIED ULTIMATE STRENGTH f_{UTA}	MINIMUM SPECIFIED YIELD STRENGTH 0.2% OFFSET, f _{YA}	f _{UTA} f _{YA}	MINIMUM ELONGATION, PERCENT	MINIMUM REDUCTION OF AREA, PERCENT	SPECIFICATION FOR NUTS ⁴
ASTM F 593 ² CW1 (316) 1/4 to 5/8 in.	psi (MPa)	100,000	65,000 (450)	1.54	20		F 594
ASTM F 593 ² CW2 (316) 3/ ₄ to 1 ¹ / ₂ in.	psi (MPa)	85,000 (585)	45,000 (310)	1.89	25	_	F 594
ISO 3506-1 ³ A4-70 M8 – M24	MPa (psi)	700 (101,500)	450 (65,250)	1.56	40	_	ISO 4032

¹ Hilti HIT-HY 150 MAX-SD may be used in conjunction with all grades of continuously threaded stainless steel rod (all-thread) that comply with the code reference standards and that have thread characteristics comparable with ANSI B1.1 UNC Coarse Thread Series or ANSI B1.13M M Profile Metric Thread Series. Values for threaded rod types and associated nuts supplied by Hilti are provided here.

² Standard Specification for Alloy-Steel and Stainless Steel Bolting Materials for High-Temperature Service

³ Standard Specification for Carbon and Alloy Steel Externally Threaded Metric Fasteners

⁴ Mechanical properties of fasteners made of carbon steel and alloy steel – Part 1: Bolts, screws and studs

⁵ Based on 2-in. (50 mm) gauge length except ASTM A 193, which are based on a gauge length of 4d and ISO 898 which is based on 5d. ⁶ Nuts of other grades and styles having specified proof load stresses greater than the specified grade and style are also suitable. Nuts must have specified proof load stresses equal to or greater than the minimum tensile strength of the specified threaded rod.

⁷ Nuts for fractional rods.

² Standard Steel Specification for Stainless Steel Bolts, Hex Cap Screws, and Studs

³ Mechanical properties of corrosion-resistant stainless steel fasteners – Part 1: Bolts, screws and studs

⁴ Nuts of other grades and styles having specified proof load stresses greater than the specified grade and style are also suitable. Nuts must have specified proof load stresses equal to or greater than the minimum tensile strength of the specified threaded rod.

TABLE 4—TENSILE PROPERTIES OF COMMON REINFORCING BARS

REINFORCING BAR SPECIFICATIO	N	MINIMUM SPECIFIED ULTIMATE STRENGTH, f_{uta}	MINIMUM SPECIFIED YIELD STRENGTH, f_{ya}
ASTM A 615 ¹ Gr. 60	psi	90,000	60,000
ASTMACTS GL. 60	(MPa)	(620)	(415)
ASTM A 615 ¹ Gr. 40	psi	60,000	40,000
ASTM A 615 GI. 40	(MPa)	(415)	(275)
DIN 488 ² BSt 500	MPa	550	500
DIN 400 BSI 500	(psi)	(79,750)	(72,500)
CAN/CSA-G30.18 ³ Gr. 400	MPa	540	400
CAN/CSA-G30.18 Gf. 400	(psi)	(78,300)	(58,000)

Standard Specification for Deformed and Plain Carbon Steel Bars for Concrete Reinforcement
 Reinforcing steel; reinforcing steel bars; dimensions and masses
 Billet-Steel Bars for Concrete Reinforcement

TABLE 5—STEEL DESIGN INFORMATION FOR FRACTIONAL THREADED ROD1

					NON	IINAL ROD D	IAMETER (inc	ches)			
	DESIGN INFORMATION	SYMBOL	UNITS	³ / ₈	¹ / ₂	⁵ / ₈	3/4	⁷ / ₈	1		
D!	0.0	-1	in.	0.375	0.5	0.625	0.75	0.875	1		
Roa	O.D.	d	(mm)	(9.5)	(12.7)	(15.9)	(19.1)	(22.2)	(25.4)		
Dod	offective erose sectional area	4	in. ²	0.0775	0.1419	0.2260	0.3345	0.4617	0.6057		
Roa	effective cross-sectional area	A _{se}	(mm²)	(50)	(92)	(146)	(216)	(298)	(391)		
		M	lbf	5,620	10,290	16,385	24,250	33,470	43,910		
	Nominal strength as	N _{sa}	(kN)	(25.0)	(45.8)	(72.9)	(107.9)	(148.9)	(195.3)		
s 5.8	governed by steel strength	V	lbf	2,810	6,175	9,830	14,550	20,085	26,345		
Clas		V _{sa}	(kN)	(12.5)	(27.5)	(43.7)	(64.7)	(89.3)	(117.2)		
SO 898-1 Class	Reduction for seismic shear	$a_{V,seis}$	-			0	.7				
ISO	Strength reduction factor ϕ for tension ²	φ	-			0.	65				
	Strength reduction factor ϕ for shear ²	φ	-			0.	60				
		Δ/	lbf	9,690	17,740	28,250	41,810	57,710	75,710		
	Nominal strength as	N _{sa}	(kN)	(43.1)	(78.9)	(125.7)	(186.0)	(256.7)	(336.8)		
22	governed by steel strength	1/	lbf	4,845	10,640	16,950	25,090	34,630	45,425		
193 E		V _{sa}	(kN)	(21.5)	(47.3)	(75.4)	(111.6)	(154.0)	(202.1)		
ASTM A 193 B7	Reduction for seismic shear	$a_{V,seis}$	-			0	.7				
AS	Strength reduction factor ϕ for tension ³	φ	-			0.	75				
	Strength reduction factor ϕ for shear ³	φ	-			0.	65				
			lbf	7,750	14,190	22,600	28,430	39,245	51,485		
SS	Nominal strength as	N _{sa}	(kN)	(34.5)	(63.1)	(100.5)	(126.5)	(174.6)	(229.0)		
ainle	governed by steel strength		lbf	3,875	8,515	13,560	17,060	23,545	30,890		
N St		V _{sa}	(kN)	(17.2)	(37.9)	(60.3)	(75.9)	(104.7)	(137.4)		
593, C\	Reduction for seismic shear	$a_{V,seis}$	-	0.7							
ASTM F 593, CW Stainless	Strength reduction factor ϕ for tension ²	φ	-	0.65							
ĕ	Strength reduction factor ϕ for shear ²	φ	-			0.	60				

¹ Values provided for common rod material types based on published strengths and calculated in accordance with ACI 318 Eq. (D-3) and Eq. (D-20). Other material specifications are admissible, subject to the approval of the code official. Nuts and washers must be appropriate for the rod strength.

² For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of ϕ must be determined in accordance with ACI 318 D.4.5. Values correspond to a brittle steel element.

³ For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of

 $^{^3}$ For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of ϕ must be determined in accordance with ACI 318 D.4.5. Values correspond to a ductile steel element.

TABLE 6—CONCRETE BREAKOUT DESIGN INFORMATION FOR FRACTIONAL THREADED ROD1

DEGION INFORMATION	0.44501			NON	INAL ROD D	IAMETER (inc	hes)	
DESIGN INFORMATION	SYMBOL	UNITS	³ / ₈	1/2	⁵ / ₈	3/4	⁷ / ₈	1
Effectiveness factor for uncracked	le.	in-lb	24	24	24	24	27	27
concrete	$k_{c,uncr}$	(SI)	(10)	(10)	(10)	(10)	(11.3)	(11.3)
Effectiveness factor for cracked	l.	in-lb	17	17	17	17	17	17
concrete	$K_{c,cr}$	(SI)	(7)	(7)	(7)	(7)	(7)	(7)
Min. anchor spacing⁴	•	in.	1 ⁷ / ₈	21/2	3 ¹ / ₈	3 ³ / ₄	4 ³ / ₈	5
Will. allerior spacing	S _{min}	(mm)	(48)	(64)	(79)	(95)	(111)	(127)
Min. edge distance⁴	•	in.	1 ⁷ / ₈	21/2	3 ¹ / ₈	3 ³ / ₄	4 ³ / ₈	5
wiin. edge distance	C _{min}	(mm)	(48)	(64)	(79)	(95)	(111)	(127)
Minimum member thickness	h _{min}	in. (mm)		+ 1 ¹ / ₄ + 30)		h _{ef} +	2d ₀ ⁽³⁾	
Critical edge distance – splitting (for uncracked concrete)	C _{ac}	1		S	ee Section 4.1.	.10 of this repo	ort.	
Strength reduction factor for tension, concrete failure modes, Condition B ²	φ	-			0.	65		
Strength reduction factor for shear, concrete failure modes, Condition B ²	φ	-			0.	70		

¹ For additional setting information, see installation instructions in Figure 5.

 $^{^2}$ Values provided for post-installed anchors with category as determined from ACI 355.2 given for Condition B. Condition B applies without supplementary reinforcement or where pullout (bond) or pryout govern, as set forth in ACI 318 D.4.4, while condition A requires supplemental reinforcement. Values are for use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of ϕ must be determined in accordance with ACI 318 D.4.5.

 $^{^{3}}d_{0}$ = hole diameter.

⁴For installations with 1³/₄ inch edge distance, refer to Section 4.1.9 for spacing and maximum torque requirements.

TABLE 7—BOND STRENGTH DESIGN INFORMATION FOR FRACTIONAL THREADED ROD1

	DE0	ION INFORMATION	OVMDOL	LINUTO		NC	OMINAL ROD	DIAMETER (I	N.)	
	DES	IGN INFORMATION	SYMBOL	UNITS	³ / ₈	1/2	⁵ / ₈	3/4	⁷ / ₈	1
		Characteristic bond		psi	1,985	1,985	1,850	1,710	1,575	1,440
	_	strength in uncracked concrete	$ au_{k,uncr}$	(MPa)	(13.7)	(13.7)	(12.7)	(11.8)	(10.9)	(9.9)
	Α	Characteristic bond strength in cracked	_	psi	696	763	821	881	889	896
~		concrete ³	$ au_{k,cr}$	(MPa)	(4.8)	(5.3)	(5.7)	(6.1)	(6.1)	(6.2)
Range ²		Characteristic bond strength in uncracked	-	psi	1,610	1,610	1,495	1,385	1,275	1,170
le R	Concrete Characteristic bond strength in cracked concrete³	$ au_{k,uncr}$	(MPa)	(11.1)	(11.1)	(10.3)	(9.6)	(8.8)	(8.1)	
eratu		_	psi	561	615	662	711	717	723	
emp		concrete ³	$ au_{k,cr}$	(MPa)	(3.9)	(4.2)	(4.6)	(4.9)	(4.9)	(5.0)
		Characteristic bond strength in uncracked	τ	psi	930	930	865	805	740	675
	С	concrete	$ au_{k,uncr}$	(MPa)	(6.4)	(6.4)	(6.0)	(5.5)	(5.1)	(4.7)
		Characteristic bond strength in cracked concrete ³	_	psi	321	352	379	407	410	414
			$ au_{k,cr}$	(MPa)	(2.2)	(2.4)	(2.6)	(2.8)	(2.8)	(2.9)
N 41				in.	2 ³ / ₈	2 ³ / ₄	3 ¹ / ₈	3 ¹ / ₂	3 ¹ / ₂	4
Minir	num	anchor embedment depth	h _{ef,min}	(mm)	(60)	(70)	(79)	(89)	(89)	(102)
			,	in.	7 ¹ / ₂	10	12 ¹ / ₂	15	17 ¹ / ₂	20
IVIaxii	Maximum anchor embedment depth		h _{ef,max}	(mm)	(191)	(254)	(318)	(381)	(445)	(508)
Permissible Installation	Conditions	Dry concrete & Water-	Anchor Category	-			,	1		
Permi	Cond	saturated concrete	φ _d & φ _{ws}				0.	65		

For **SI**: 1 inch \equiv 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 MPa.

¹ Bond strength values correspond to concrete compressive strength range 2,500 psi $\leq f_c \leq 4,500$ psi. For 4,500 psi $\leq f_c \leq 6,500$ psi, tabulated characteristic bond strengths may be increased by 6 percent. For 6,500 psi < f'c \le 8,000 psi, tabulated characteristic bond strengths may be increased by 10 percent.

² Temperature range A: Maximum short term temperature = 104°F (40°C), maximum long term temperature = 75°F (24°C).

Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C). Temperature range C: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 162°F (72°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³For structures assigned to Seismic Design Categories C, D, E or F, bond strength values are multiplied by $\alpha_{N,seis}$ = 1.0 => no reduction.

TABLE 8—STEEL DESIGN INFORMATION FOR METRIC THREADED ROD1

	DESIGN INFORMATION	SYMBOL	UNITS		NOMINA	ROD DIAME	TER (mm)		
	DESIGN INFORMATION	STWIDOL	UNITS	10	12	16	20	24	
D - 1		-1	mm	10	12	16	20	24	
Rod (J.D.	d	(in.)	(0.39)	(0.47)	(0.63)	(0.79)	(0.94)	
Dod	effective cross-sectional area	4	mm ²	58	84.3	157	245	353	
Rou e	enective cross-sectional area	A_{se}	(in. ²)	(0.090)	(0.131)	(0.243)	(0.380)	(0.547)	
		N _{sa}	kN	29.0	42.2	78.5	122.5	176.5	
ω.	Nominal strength as governed by	IVsa	(lb)	(6,520)	(9,475)	(17,650)	(27,540)	(39,680)	
ss 5	steel strength	V_{sa}	kN	14.5	25.3	47.1	73.5	105.9	
Class 5.		v sa	(lb)	(3,260)	(5,685)	(10,590)	(16,525)	(23,810)	
4	Reduction for seismic shear	$a_{V,seis}$	-			0.7			
SO 898-1	Strength reduction factor ϕ for tension ²	φ	-	- 0.65					
<u>0)</u>	Strength reduction factor ϕ for shear ²	φ	-			0.60			
	Nominal strength as governed by steel strength		kN	46.4	67.4	125.6	196.0	282.4	
œ.		N _{sa}	(lb)	(10,430)	(15,160)	(28,235)	(44,065)	(63,485)	
88		1/	kN	23.2	40.5	75.4	117.6	169.4	
Class		V_{sa}	(lb)	(5,215)	(9,100)	(16,940)	(26,440)	(38,090)	
898-1	Reduction for seismic shear	$a_{V,seis}$	-			0.7			
368 OSI	Strength reduction factor ϕ for tension ²	φ	-			0.65			
<u>0)</u>	Strength reduction factor ϕ for shear ²	φ	-			0.60			
e		A.1	kN	40.6	59.0	109.9	171.5	247.1	
SS	Nominal strength as governed by	N _{sa}	(lb)	(9,130)	(13,263)	(24,703)	(38,555)	(55,550)	
A4	steel strength	17	kN	20.3	35.4	65.9	102.9	148.3	
ass		V_{sa}	(lb)	(4,565)	(7,960)	(14,825)	(23,135)	(33,330)	
<u>0</u>	Reduction for seismic shear	$a_{V,seis}$	-	0.7					
3506-1 Class A4 SS ³	Strength reduction factor ϕ for tension ²	φ	-			0.65			
180	Strength reduction factor ϕ for shear ²	φ	-			0.60			

¹ Values provided for common rod material types based on published strengths and calculated in accordance with ACI 318 Eq. (D-3) and Eq. (D-20). Other material specifications are admissible, subject to the approval of the code official. Nuts and washers must be appropriate for the rod strength.

² For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of *φ* must be determined in accordance with ACI 318 D.4.5. Values correspond to a brittle steel element.

³ A4-70 Stainless (M10 - M24 diameters).

TABLE 9—CONCRETE BREAKOUT DESIGN INFORMATION FOR METRIC THREADED ROD1

DESIGN INFORMATION	SYMBOL	UNITS		NOMINAL ROD DIAMETER (mm)			
DESIGN INFORMATION	STWIBOL	UNITS	10	12	16	20	24
Effectiveness factor for uncracked	l.	SI	10	10	10	10	11.3
concrete	$k_{c,uncr}$	(in-lb)	(24)	(24)	(24)	(24)	(27)
Effectiveness factor for cracked concrete	k	SI	7	7	7	7	7
Effectiveness factor for cracked concrete	$k_{c,cr}$	(in-lb)	(17)	(17)	(17)	(17)	(17)
Min anchar angaing ⁴	_	mm	50	60	80	100	120
Min. anchor spacing⁴	S _{min}	(in.)	(2.0)	(2.4)	(3.2)	(3.9)	(4.7)
Min. edge distance ⁴	•	mm	50	60	80	100	120
iviiri. euge distance	C _{min}	(in.)	(2.0)	(2.4)	(3.2)	(3.9)	(4.7)
Minimum member thickness	h	mm	h _{ef} + 30	$h_{\rm ef} + 2d_0^{(3)}$			
Millimum member unckness	h _{min}	(in.)	$(h_{ef} + 1^1/_4)$		∏ _{ef} ⊤	2U ₀	
Critical edge distance – splitting (for uncracked concrete)	C _{ac}	-		See Sec	tion 4.1.10 of th	nis report.	
Strength reduction factor for tension, concrete failure modes, Condition B ²	φ	-	- 0.65				
Strength reduction factor for shear, concrete failure modes, Condition B ²							

For **SI:** 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897 Mpa

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

 $^{3}d_{0}$ = drill bit diameter.

¹ For additional setting information, see installation instructions in Figure 5.

² Values provided for post-installed anchors with category as determined from ACI 355.2 given for Condition B. Condition B applies without supplementary reinforcement or where pullout (bond) or pryout govern, as set forth in ACI 318 D.4.4, while condition A requires supplemental reinforcement. Values are for use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of ϕ must be determined in accordance with ACI 318 D.4.5.

⁴For installations with 1³/₄ inch edge distance, refer to Section 4.1.9 for spacing and maximum torque requirements.

TABLE 10—BOND STRENGTH DESIGN INFORMATION FOR METRIC THREADED ROD1

	Di	ESIGN INFORMATION	SYMBOL	UNITS		NOMINA	ROD DIAME	TER (mm)	
	Di	231314 INI OKMATION	STWIDOL	UNITS	10	12	16	20	24
		Characteristic bond strength in		MPa	13.7	13.7	12.7	11.8	10.9
		uncracked concrete	$ au_{k,uncr}$	(psi)	(1,985)	(1,985)	(1,850)	(1,710)	(1,575)
	Α	Characteristic bond strength in		MPa	4.9	5.1	5.7	6.1	6.2
80		cracked concrete ³	$ au_{k,cr}$	(psi)	(705)	(744)	(822)	(884)	(893)
Temperature Range ²		Characteristic bond strength in		MPa	11.1	11.1	10.3	9.6	8.8
ē R		uncracked concrete	$ au_{k,uncr}$	(psi)	(1,610)	(1,610)	(1,500)	(1,390)	(1,275)
ratu	В	Characteristic bond strength in cracked concrete ³		MPa	3.9	4.1	4.6	4.9	5.0
edu			$ au_{k,cr}$	(psi)	(569)	(600)	(663)	(712)	(720)
Te		Characteristic bond strength in uncracked concrete	_	MPa	6.4	6.4	6.0	5.5	5.1
			$ au_{k,uncr}$	(psi)	(930)	(930)	(865)	(805)	(740)
	С	Characteristic bond strength in		MPa	2.2	2.4	2.6	2.8	2.8
		cracked concrete ³	$ au_{k,cr}$	(psi)	(326)	(343)	(379)	(408)	(412)
Minima			L	mm	60	70	80	90	96
IVIIIIIII	ım aı	nchor embedment depth	$h_{\it ef,min}$	(in.)	(2.4)	(2.8)	(3.1)	(3.5)	(3.8)
Mavim		anahar amhadmant danth	h	mm	200	240	320	400	480
IVIAXIIII	aximum anchor embedment depth		h _{ef,max}	(in.)	(7.9)	(9.4)	(12.6)	(15.7)	(18.9)
Permissible Installation	Conditions	Dry concrete & Water-	Anchor Category	,			1		
Perm	Con	saturated concrete	ϕ_d & ϕ_{ws}	-			0.65		

¹ Bond strength values correspond to concrete compressive strength range 2,500 psi $\leq f_c \leq 4,500$ psi. For 4,500 psi $\leq f_c \leq 6,500$ psi, tabulated characteristic bond strengths may be increased by 6 percent. For 6,500 psi < f'_c \le 8,000 psi, tabulated characteristic bond strengths may be increased by 10 percent.

² Temperature range A: Maximum short term temperature = 104°F (40°C), maximum long term temperature = 75°F (24°C). Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C).

Temperature range C: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 162°F (72°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³For structures assigned to Seismic Design Categories C, D, E or F, bond strength values are multiplied by αN,seis = 1.0 => no reduction.

TABLE 11—STEEL DESIGN INFORMATION FOR U.S. IMPERIAL REINFORCING BARS¹

	DESIGN INFORMATION	SYMBOL	UNITS			BAR	SIZE			
	DESIGN IN ORMATION	STWIDOL	Johnson	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	
Nomi	inal bar diameter	d	in.	³ / ₈	1/2	⁵ / ₈	3/4	⁷ / ₈	1	
NOITI	mai bai diameter	u	(mm)	(9.5)	(12.7)	(15.9)	(19.1)	(22.2)	(25.4)	
Porc	effective cross-sectional area	Λ	in. ²	0.11	0.2	0.31	0.44	0.6	0.79	
ваг е	enective cross-sectional area	A _{se}	(mm ²)	(71)	(129)	(200)	(284)	(387)	(510)	
		M	lb	6,600	12,000	18,600	26,400	36,000	47,400	
40	Nominal strength as governed	N _{sa}	(kN)	(29.4)	(53.4)	(82.7)	(117.4)	(160.1)	(210.9)	
Gr. 4	by steel strength	1/	lb	3,960	7,200	11,160	15,840	21,600	28,440	
5		V_{sa}	(kN)	(17.6)	(32.0)	(49.6)	(70.5)	(96.1)	(126.5)	
A 615	Reduction for seismic shear	$\alpha_{V,seis}$	-	- 0.7						
ASTM /	Strength reduction factor ϕ for tension ²	φ	-	0.65						
∢	Strength reduction factor ϕ for shear ²	φ	-			0.	60			
		A./	lb	9,900	18,000	27,900	39,600	54,000	71,100	
09	Nominal strength as governed	N _{sa}	(kN)	(44.0)	(80.1)	(124.1)	(176.2)	(240.2)	(316.3)	
Gr. 6	by steel strength	1/	lb	5,940	10,800	16,740	23,760	32,400	42,660	
5		V_{sa}	(kN)	(26.4)	(48.0)	(74.5)	(105.7)	(144.1)	(189.8)	
۸ 615	Reduction for seismic shear	α _{V,seis}	-			0	.7			
ASTM A	Strength reduction factor ϕ for tension ²	φ	-			0.	65			
∢	Strength reduction factor ϕ for shear ²	φ	-			0.	60			

¹ Values provided for common rod material types based on published strengths and calculated in accordance with ACI 318 Eq. (D-3) and Eq. (D-20). Other material specifications are admissible, subject to the approval of the code official. Nuts and washers must be appropriate for the rod strength.

² For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of *ϕ* must be determined in accordance with ACI 318 D.4.5. Values correspond to a brittle steel element.

TABLE 12—CONCRETE BREAKOUT DESIGN INFORMATION FOR U.S. IMPERIAL REINFORCING BARS1

DESIGN INFORMATION	SYMBOL	UNITS			BAR	SIZE				
DESIGN IN ORMATION	STWIDOL	ONITS	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8		
Effectiveness factor for uncracked	k	in-lb	24	24	24	24	24	24		
concrete	K _{c,uncr}	(SI)	(10)	(10)	(10)	(10)	(10)	(10)		
Effectiveness factor for cracked	k	in-lb	17	17	17	17	17	17		
concrete	K _{c,cr}	(SI)	(7)	(7)	(7)	(7)	(7)	(7)		
Min. bar spacing ⁴		in.	1 ⁷ / ₈	21/2	3 ¹ / ₈	3 ³ / ₄	4 ³ / ₈	5		
IVIIII. bar spacing	S _{min}	(mm)	(48)	(64)	(79)	(95)	(111)	(127)		
Min. edge distance ⁴	C _{min}	in.	1 ⁷ / ₈	21/2	3 ¹ / ₈	3 ³ / ₄	4 ³ / ₈	5		
iviiii. eage distance		(mm)	(48)	(64)	(79)	(95)	(111)	(127)		
Minimum member thickness	6	in.	$h_{ef} + 1^{1}/_{4}$ $(h_{ef} + 30)$		$h_{ef} + 2d_0^{(3)}$					
Willimum member unickness	h _{min}	(mm)			$n_{\rm ef} + 2a_0$					
Critical edge distance – splitting (for uncracked concrete)	Cac	-		Se	e Section 4.1	.10 of this rep	0 of this report.			
Strength reduction factor for tension, concrete failure modes, Condition B ²	φ	-			0.	0.65				
Strength reduction factor for shear, concrete failure modes, Condition B ²	φ	-		0.70						

¹ For additional setting information, see installation instructions in Figure 5.

² Values provided for post-installed anchors with category as determined from ACI 355.2 given for Condition B. Condition B applies without supplementary reinforcement or where pullout (bond) or pryout govern, as set forth in ACI 318 D.4.4, while condition A requires supplemental reinforcement. Values are for use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of *φ* must be determined in accordance with ACI 318 D.4.5.

 $^{^{3}}d_{0}$ = drill bit diameter.

⁴For installations with 1³/₄ inch edge distance, refer to Section 4.1.9 for spacing and maximum torque requirements.

TABLE 13—BOND STRENGTH DESIGN INFORMATION FOR U.S. IMPERIAL REINFORCING BARS1

	DESIG	SN INFORMATION	SYMBOL	UNITS			BAR	SIZE			
	LOIC	SIN IN ORMATION	STWIDOL	ONITS	No. 3	No. 4	No. 5	No. 6	No. 7	No. 8	
		Characteristic bond	_	psi			1,2	90			
	Α	strength in uncracked concrete	$ au_{k,uncr}$	MPa			(8.	.9)			
	A	Characteristic bond strength in cracked	_	psi	696	763	821	881	889	896	
₂ 0		concrete ³	$ au_{k,cr}$	MPa	(4.8)	(5.3)	(5.7)	(6.1)	(6.1)	(6.2)	
ange		Characteristic bond	_	psi	1,045						
Temperature Range ²	В	strength in uncracked concrete	$ au_{k,uncr}$	MPa			(7.	.2)			
eratu	В	Characteristic bond		psi	561	615	662	711	717	723	
e duic		strength in cracked concrete ³	$ au_{k,cr}$	MPa	(3.9)	(4.2)	(4.6)	(4.9)	(4.9)	(5.0)	
Ĭ		Characteristic bond		psi			60)5			
		strength in uncracked concrete	$ au_{k,uncr}$	MPa			(4.	.2)			
	С	Characteristic bond		psi	321	352	379	407	410	414	
		strength in cracked concrete ³	$ au_{k,cr}$	MPa	(2.2)	(2.4)	(2.6)	(2.8)	(2.8)	(2.9)	
Minim	ıım aı	nchor embedment depth	h _{ef.min}	in.	2 ³ / ₈	2 ³ / ₄	3 ¹ / ₈	3 ¹ / ₂	3 ¹ / ₂	4	
	aiii ai	ionor embeament deptir	i er,min	(mm)	(60)	(70)	(79)	(89)	(89)	(102)	
Maxim	num a	inchor embedment	h	in.	$7^{1}/_{2}$	10	12 ¹ / ₂	15	17 ¹ / ₂	20	
depth			h _{ef,max}	(mm)	(191)	(254)	(318)	(381)	(445)	(508)	
Permissible Installation	ditions	Dry concrete & Water-saturated concrete	Anchor Category	-			•	1			
Pern	Con	Saturated concrete	ϕ_d & ϕ_{ws}	-			0.0	65			

¹ Bond strength values correspond to concrete compressive strength range 2,500 psi $\leq f_c \leq$ 4,500 psi. For 4,500 psi $< f_c \leq$ 6,500 psi, tabulated characteristic bond strengths may be increased by 6 percent. For 6,500 psi < f'c \leq 8,000 psi, tabulated characteristic bond strengths may be increased by 10 percent.

² Temperature range A: Maximum short term temperature = 104°F (40°C), maximum long term temperature = 75°F (24°C). Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C). Temperature range C: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 162°F (72°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

 $^{^{3}}$ For structures assigned to Seismic Design Categories C, D, E or F, bond strength values are multiplied by αN , seis = 1.0 => no reduction.

TABLE 14—STEEL DESIGN INFORMATION FOR EU METRIC REINFORCING BARS1

	DESIGN INFORMATION	SYMBOL	SYMBOL UNITS BAR SIZE		SIZE				
	DESIGN IN CHIMATION	OTHIDOL	OMITO	10	12	14	16	20	25
Nami	nal bar diameter	d	mm	10.0	12.0	14.0	16.0	20.0	25.0
NOTTI	lai bar diameter	ŭ	(in.)	(0.394)	(0.472)	(0.551)	(0.630)	(0.787)	(0.984)
Dono	factive gross sectional gross	A _{se}	mm ²	78.5	113.1	153.9	201.1	314.2	490.9
ваг е	ffective cross-sectional area		(in. ²)	(0.122)	(0.175)	(0.239)	(0.312)	(0.487)	(0.761)
		N _{sa}	kN	43.2	62.2	84.7	110.6	172.8	270.0
8	Nominal strength as governed by		(lb)	(9,710)	(13,985)	(19,035)	(24,860)	(38,845)	(60,695)
550/500	steel strength		kN	25.9	37.3	50.8	66.4	103.7	162.0
t 55			(lb)	(5,830)	(8,390)	(11,420)	(14,915)	(23,310)	(36,415)
BSt	Reduction for seismic shear	Reduction for seismic shear $\alpha_{V,seis}$		0.7					
DIN 488	Strength reduction factor ϕ for tension ²	φ	-						
۵	Strength reduction factor ϕ for shear ²	φ	-		0.60				

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

TABLE 15—CONCRETE BREAKOUT DESIGN INFORMATION FOR EU METRIC REINFORCING BARS1

DESIGN INFORMATION	SYMBOL	UNITS			BAR SIZE				
DEGIGN IN ORMATION	STWIDOL	OMITO	10	12	14	16	20	25	
Effectiveness factor for uncracked	k	SI			10			12.6	
concrete	k _{c,uncr}	(in-lb)			(24)			(30)	
Effectiveness factor for cracked	K _{c.cr}	SI				7			
concrete	K _{C,C}	(in-lb)			(1	7)			
Min. bar spacing ⁴		mm	50	60	70	80	100	125	
Willi. Dai Spacing	S _{min}	(in.)	(2)	(2.4)	(2.8)	(3.1)	(3.9)	(4.9)	
Min. edge distance ⁴	C _{min}	mm	50	60	70	80	100	125	
lviiii. edge distance		(in.)	(2)	(2.4)	(2.8)	(3.1)	(3.9)	(4.9)	
Minimum member thickness	h	mm	$h_{ef} + 30$	$h_{ef} + 2d_0^{(3)}$					
Willimitati member triickness	h _{min}	(in.)	$(h_{ef} + 1^{1}/_{4})$	$n_{\text{ef}} + 2d_0^{(c)}$					
Critical edge distance – splitting (for uncracked concrete)	C _{ac}	-	- See Section 4.1.10 of this report.						
Strength reduction factor for tension, concrete failure modes, Condition B ²	or tension, ondition B^2 ϕ - 0.65								
Strength reduction factor for shear, concrete failure modes, Condition B ²	φ	-			0.	70			

For **SI:** 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

¹ Values provided for common rod material types based on published strengths and calculated in accordance with ACI 318 Eq. (D-3) and Eq. (D-20). Other material specifications are admissible, subject to the approval of the code official. Nuts and washers must be appropriate for the rod strength.

² For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of *φ* must be determined in accordance with ACI 318 D.4.5. Values correspond to a brittle steel element.

¹ For additional setting information, see installation instructions in Figure 5.

² Values provided for post-installed anchors with category as determined from ACI 355.2 given for Condition B. Condition B applies without supplementary reinforcement or where pullout (bond) or pryout govern, as set forth in ACI 318 D.4.4, while condition A requires supplemental reinforcement. Values are for use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C or are used, the appropriate value of *ϕ* must be determined in accordance with ACI 318 D.4.5.

 $^{{}^{3}}d_{0}$ = drill bit diameter.

⁴For installations with 1³/₄ inch edge distance, refer to Section 4.1.9 for spacing and maximum torque requirements.

TABLE 16—BOND STRENGTH DESIGN INFORMATION FOR EU METRIC REINFORCING BARS1

	DE	SIGN INFORMATION	SYMBOL	UNITS			BAR	SIZE			
	DE.	SIGN INFORMATION	STWIBOL	UNITS	10	12	14	16	20	25	
		Characteristic bond		MPa			8	.9			
	A	strength in uncracked concrete	T _{k, uncr}	(psi)			(1,2	290)			
	A	Characteristic bond		MPa	4.9	5.1	5.4	5.7	6.1	6.2	
8		strength in cracked concrete ³	$ au_{k,cr}$	(psi)	(705)	(744)	(783)	(822)	(884)	(895)	
ange		Characteristic bond		MPa	7.2						
Temperature Range ²		strength in uncracked concrete	$ au_{k,uncr}$	(psi)			(1,0	045)			
ratu	В	Characteristic bond		MPa	3.9	4.1	4.4	4.6	4.9	5.0	
edus		strength in cracked concrete ³	$ au_{k,cr}$	(psi)	(569)	(600)	(631)	(663)	(712)	(722)	
Ĭ,		Characteristic bond		MPa		4.2					
		strength in uncracked concrete	$ au_{k,uncr}$	(psi)			(6	05)			
	С	Characteristic bond		MPa	2.2	2.4	2.5	2.6	2.8	2.9	
		strength in cracked concrete ³	$ au_{k,cr}$	(psi)	(326)	(343)	(361)	(379)	(408)	(413)	
Minim		nobor ombodment denth	6	mm	60	70	75	80	90	100	
IVIIIIIIII	um a	nchor embedment depth	h _{ef,min}	(in.)	(2.4)	(2.8)	(3.0)	(3.1)	(3.5)	(3.9)	
Movim	Maximum anchor embedment depth		h	mm	200	240	280	320	400	500	
Maxim	iuiii a	anchor embedment depth	h _{ef,max}	(in.)	(7.9)	(9.4)	(11.0)	(12.6)	(15.7)	(19.7)	
Permissible Installation	Conditions	Dry concrete & Water-saturated concrete	Anchor Category	-				1			
Perm	Con	Saturated Concrete	φ _d & φ _{ws}	-			0.	65			

¹ Bond strength values correspond to concrete compressive strength range 2,500 psi $\leq f_c \leq$ 4,500 psi. For 4,500 psi $< f_c \leq$ 6,500 psi, tabulated characteristic bond strengths may be increased by 6 percent. For 6,500 psi < f'c \leq 8,000 psi, tabulated characteristic bond strengths may be increased by 10 percent.

² Temperature range A: Maximum short term temperature = 104°F (40°C), maximum long term temperature = 75°F (24°C). Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C). Temperature range C: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 162°F (72°C).

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³For structures assigned to Seismic Design Categories C, D, E or F, bond strength values are multiplied by $\alpha_{N,seis}$ = 1.0 => no reduction.

TABLE 17—STEEL DESIGN INFORMATION FOR CANADIAN METRIC REINFORCING BARS1

	DESIGN INFORMATION	SYMBOL	UNITS		BAR	SIZE			
· '	DEGICIA INI ORIMATION	OTHIDOL	ONITO	10 M	15 M	20 M	25 M		
Nom	inal bar diameter	م	mm	11.3	16.0	19.5	25.2		
NOITI	mai par diameter	d	(in.)	(0.445)	(0.630)	(0.768)	(0.992)		
Done	effective group sectional group	4	mm ²	100.3	201.1	298.6	498.8		
Bare	effective cross-sectional area	A _{se}	(in.²)	(0.155)	(0.312)	(0.463)	(0.773)		
		Α./	kN	54.2	108.6	161.3	269.3		
400	Nominal strength as governed by steel strength	N _{sa}	(lb)	(12,175)	(24,410)	(36,255)	(60,550)		
		V _{sa}	kN	32.5	65.1	96.8	161.6		
8 Gr.			(lb)	(7,305)	(14,645)	(21,755)	(36,330)		
0.1	Reduction for seismic shear	$a_{V,seis}$	-	0.7					
CSA-G30.18	Strength reduction factor ϕ for tension ²	φ	-		0.	0.65			
Ö	Strength reduction factor ϕ for shear ²	φ	-		0.	60			

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

TABLE 18—CONCRETE BREAKOUT DESIGN INFORMATION FOR CANADIAN METRIC REINFORCING BARS1

DESIGN INFORMATION	SYMBOL	UNITS		BAI	BAR SIZE			
DESIGN INFORMATION	STWIBOL	UNITS	10 M	15 M	20 M	25 M		
Effectiveness factor for uncracked	l.	SI	10	10	10	11.3		
concrete	k _{c,uncr}	(in-lb)	(24)	(24)	(24)	(27)		
Effectiveness factor for cracked	l.	SI	7	7	7	7		
concrete	$k_{c,cr}$	(in-lb)	(17)	(17)	(17)	(17)		
Min har angaing ⁴		mm	57	80	98	126		
Min. bar spacing ⁴	S _{min}	(in.)	(2.2)	(3.1)	(3.8)	(5.0)		
Min adag distance ⁴		mm	57	80	98	126		
Min. edge distance ⁴	C _{min}	(in.)	(2.2)	(3.1)	(3.8)	(5.0)		
Minimum member thickness	h	mm	h _{ef} + 30	4 . 2d ⁽³⁾				
IVIIIIIIIIIIIIIIIIIIIDEI IIIICKIIESS	h _{min}	(in.)	$(h_{ef} + 1^{1}/_{4})$	$h_{ef} + 2d_0^{(3)}$				
Critical edge distance – splitting (for uncracked concrete)	C _{ac}	-	See Section 4.1.10 of this report.					
Strength reduction factor for tension, concrete failure modes, Condition B ²	φ	-	0.65					
Strength reduction factor for shear, concrete failure modes, Condition B ²	φ	1	0.70					

For SI: 1 inch = 25.4 mm, 1 lbf = 4.448 N, 1 psi = 0.006897MPa.

¹ Values provided for common rod material types based on published strengths and calculated in accordance with ACI 318 Eq. (D-3) and Eq. (D-20). Other material specifications are admissible, subject to the approval of the code official. Nuts and washers must be appropriate for the rod strength.

² For use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of *φ* must be determined in accordance with ACI 318 D.4.5. Values correspond to a brittle steel element.

¹ For additional setting information, see installation instructions in Figure 5.

² Values provided for post-installed anchors with category as determined from ACI 355.2 given for Condition B. Condition B applies without supplementary reinforcement or where pullout (bond) or pryout govern, as set forth in ACI 318 D.4.4, while condition A requires supplemental reinforcement. Values are for use with the load combinations of IBC Section 1605.2.1 or ACI 318 Section 9.2 as set forth in ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of *φ* must be determined in accordance with ACI 318 D.4.5.

 $^{{}^{3}}d_{0}$ = drill bit diameter.

⁴For installations with 1³/₄ inch edge distance, refer to Section 4.1.9 for spacing and maximum torque requirements.

TABLE 19—BOND STRENGTH DESIGN INFORMATION FOR CANADIAN METRIC REINFORCING BARS1

	nee	IGN INFORMATION	SYMBOL	UNITS		BAR	SIZE				
'	DLJ	IGN INI ORMATION	STWIDOL	ONITS	10 M	15 M	20 M	25 M			
		Characteristic bond		MPa		8.	9				
	Α	strength in uncracked concrete	T _{k,uncr}	(psi)		(1,2	90)				
	A	Characteristic bond		MPa	4.9	5.7	6.0	6.2			
2		strength in cracked concrete ³	$ au_{k,cr}$	(psi)	(705)	(822)	(884)	(895)			
ange		Characteristic bond		MPa	7.2						
re R	Б	strength in uncracked concrete	$ au_{k,uncr}$	(psi)		(1,0	45)				
Temperature Range ²	В	Characteristic bond		MPa	3.9	4.6	4.9	5.0			
		strength in cracked concrete ³	$ au_{k,cr}$	(psi)	(569)	(663)	(712)	(722)			
Ĕ		Characteristic bond		MPa		4.2					
		strength in uncracked concrete	$ au_{k,uncr}$	(psi)		(60	05)				
	С	Characteristic bond		MPa	2.2	2.6	2.8	2.9			
		strength in cracked concrete ³	$ au_{k,cr}$	(psi)	(326)	(379)	(408)	(412)			
Minim	um (anchor embedment depth	h	mm	60	80	90	101			
IVIII III I	ulli	anchor embedment depth	h _{ef,min}	(in.)	(2.4)	(3.1)	(3.5)	(4.0)			
Maxin	num	anchor embedment	b	mm	226	320	390	504			
depth			h _{ef,max}	(in.)	(8.9)	(12.6)	(15.4)	(19.8)			
Permissible Installation	ditions	Dry concrete & Water-saturated concrete	Anchor Category	-		1					
Pern	Con	Saturated concrete	φ _d & φ _{ws}	-		0.6	65				

For pound-inch units: 1 mm = 0.03937 inches, 1 N = 0.2248 lbf, 1 MPa = 145.0 psi.

Short term elevated concrete temperatures are those that occur over brief intervals, e.g., as a result of diurnal cycling. Long term concrete temperatures are roughly constant over significant periods of time.

³For structures assigned to Seismic Design Categories C, D, E or F, bond strength values are multiplied by αN, seis = 1.0 => no reduction.



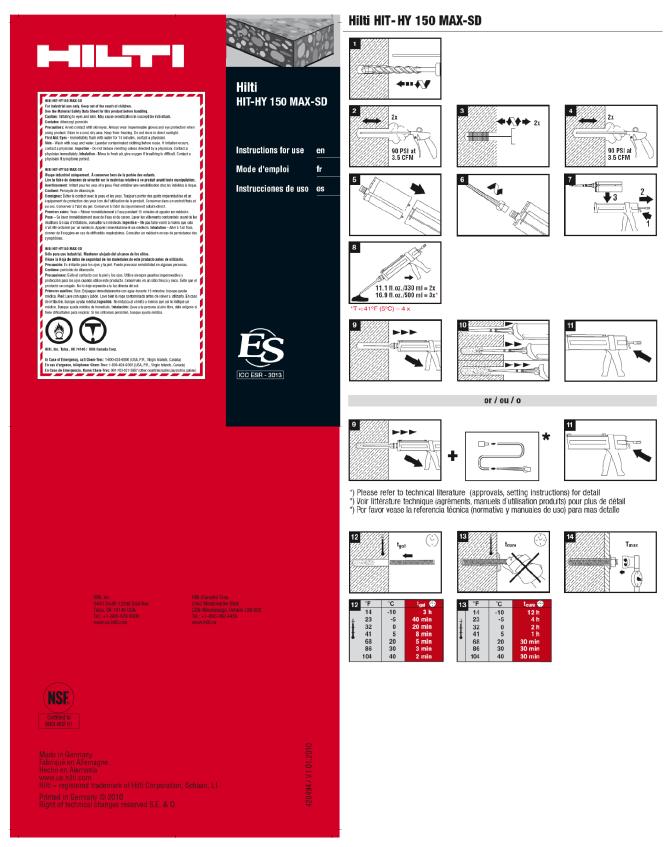
¹ Bond strength values correspond to concrete compressive strength range 2,500 psi $\leq f_c \leq 4,500$ psi. For 4,500 psi $< f_c \leq 6,500$ psi, tabulated characteristic bond strengths may be increased by 6 percent. For 6,500 psi $< f_c \leq 8,000$ psi, tabulated characteristic bond strengths may be increased by 10 percent.

² Temperature range A: Maximum short term temperature = 104°F (40°C), maximum long term temperature = 75°F (24°C). Temperature range B: Maximum short term temperature = 176°F (80°C), maximum long term temperature = 122°F (50°C). Temperature range C: Maximum short term temperature = 248°F (120°C), maximum long term temperature = 162°F (72°C).

Given: C_{a,min} (2) 1/2 inch diameter HIT-HY 150 MAX-SD 1/2-IN. A193 B7 ALL-THREAD — A_{Na} adhesive anchors C_{cr,Na} A_{Nc} subjected to a tension load as shown. s/2 Design objective: Calculate the design s/2 tension resistance for this configuration in accordance with C_{cr,Na} the 2006 IBC. A-A Dimensional Specifications / Assumptions: Parameters: ASTM A 193 B7 all-thread rods, UNC thread, A 563 Grade HD hex nuts; n =2 = 9 in. hef Normal weight concrete, $f_c = 4,000 \text{ psi}$ = 4 in.s Seismic Design Category (SDC) B = 2.5 in.C_{a,min} No supplementary reinforcing in accordance with ACI 318 D.1 = 12 in.Assume maximum short term (diurnal) base material temperature ≤ 100 °F = 1/2 in.Assume maximum long term base material temperature ≤ 75 °F Assume installation in dry concrete and hammer-drilled holes Assume concrete will remain uncracked for service life of anchorage ACI 318 Code Calculation per ACI 318 Appendix D and this report Report Ref. Ref. Step 1. Check minimum edge distance, anchor spacing and member thickness: $c_{min} = 2.5 \text{ in.} \le c_{a,min} = 2.5 \text{ in.}$ Ok Table 6 $s_{min} = 2.5 \text{ in.} \le s = 4 \text{ in.}$ ok Table 6 $h_{min} = h_{ef} + 1.25 \text{ in.} = 9 \text{ in.} + 1.25 \text{ in.} = 10.25 \text{ in.} \le h = 12 \text{ in. ok}$ Table 6 $h_{ef,min} \le h_{ef} \le h_{ef,max} \rightarrow 2-3/4 \text{ in.} \le 9 \text{ in.} \le 10 \text{ in,}$ ok Table 7 D.5.1.2 Step 2. Calculate steel strength: $N_{sa} = n \cdot A_{se} \cdot f_{uta}$ Eq. (D-3) A193 B7 rods are considered ductile in accordance with ACI 318-05 D.1. $\therefore \phi = 0.75$ $\therefore \phi \cdot N_{sa} = \phi \cdot n \cdot A_{se} \cdot f_{uta}$ Table 2 Eq. (D-3) $= 0.75 \cdot 2 \cdot 0.1419 in^2 \cdot 125,000 psi = 26,606 lb$ Table 5 or, using Table 5, $\therefore \phi \cdot N_{sa} = 0.75 \cdot 2 \cdot 17,740 lb = 26,610 lb$ Step 3. Determine concrete breakout strength: D.5.2.1 $N_{cbg} = \frac{A_{Nc}}{A_{Nco}} \cdot \psi_{ec,N} \cdot \psi_{ed,N} \cdot \psi_{c,N} \cdot \psi_{cp,N} \cdot N_b$ Eq. (D-5) $A_{Nc} = (3 \cdot h_{ef} + s) \cdot (1.5 \cdot h_{ef} + c_{a \min})$ $= (27 \text{ in.} + 4 \text{ in.}) \cdot (13.5 \text{ in.} + 2.5 \text{ in.}) = 496 \text{ in}^2$ ACI 318 Code Calculation in accordance with ACI 318 Appendix D and this report Report Ref. Ref. $A_{NCO} = 9 \cdot (h_{ef})^2 = 9 \cdot (9in)^2 = 729in^2$ Eq. (D-6)

$\psi_{\text{ec,N}}$ = 1.0 no eccentricity with respect to tension-loaded anchors	D.5.2.4	-
$c_{a,min} \le 1.5 \cdot h_{ef}$		
$c_{a,min} = 2.5 < 1.5 \cdot 9 \text{ in.} = 13.5 \text{ in.}$	D.5.2.5	
$\psi_{\text{ed,N}} = 0.7 + 0.3 \cdot \left(\frac{c_{\text{a,min}}}{1.5 \cdot h_{\text{ef}}}\right) = 0.7 + 0.3 \cdot \left(\frac{2.5 \text{in.}}{1.5 \cdot 9 \text{in.}}\right) = 0.756$	Eq. (D-11)	-
$\psi_{c,N} = 1.0$ uncracked concrete assumed, $(k_{c,uncr} = 24)$	D.5.2.6	Table 6
Determine c_{ac} : $\frac{h}{h_{ef}} = \frac{12 \text{ in.}}{9 \text{ in.}} = 1.33$		Section 4.1.10
Interpolate between 1.3 and 2.0 to get value of multiplier = 2.45. $c_{ac} = 2.45 \cdot h_{ef} = 2.45 \cdot 9 \text{in.} = 22.1 \text{in.}$		
For $c_{a,min} < c_{ac}$ $\psi_{cp,N} = \frac{\max \left c_{a,min}; 1.5 \cdot h_{ef} \right }{c_{ac}} = \frac{\max \left 2.5 \text{ in.}; 1.5 \cdot 9 \text{ in.} \right }{22.1 \text{ in.}} = 0.61$	D.5.2.7 Eq. (D-13)	-
$N_b = k_{c,uncr} \cdot \sqrt{f'_c} \cdot (h_{ef})^{1.5}$ = $24 \cdot \sqrt{4,000 \ psi} \cdot (9 \ in.)^{1.5} = 40,983 \ lb$	D.5.2.2 Eq. (D-7)	Table 6
$N_{cbg} = \frac{496 \text{in}^2}{729 \text{in}^2} \cdot 1.0 \cdot 0.756 \cdot 1.0 \cdot 0.611 \cdot 40,983 \text{lb} = 12,880 \text{lb}$	D.5.2.1 Eq. (D-5)	-
$\phi \cdot N_{cbg} = 0.65 \cdot 12,880 \text{lb} = 8,372 \text{lb}$	D.4.4(c)	-
Step 4. Determine bond strength: $N_{ag} = \frac{A_{Na}}{A_{Nao}} \cdot \psi_{ed,Na} \cdot \psi_{g,Na} \cdot \psi_{ec,Na} \cdot \psi_{p,Na} \cdot N_{ao}$	-	Section 4.1.4 Eq. (D-16b)
$\begin{split} s_{cr,Na} &= \min \Biggl(20 \cdot d \cdot \sqrt{\frac{\tau_{k,uncr}}{1,450 \ psi}}; 3 \cdot h_{ef} \Biggr) \\ &= 20 \cdot 0.5 \ in. \cdot \sqrt{\frac{1,985 \ psi}{1,450 \ psi}} = 11.7 \ in. \\ 3 \cdot h_{ef} &= 27 \ in. \ge 11.7 \ in. \\ \therefore s_{cr,Na} &= 11.7 \ in. \end{split}$	-	Section 4.1.4 D.5.3.8 Eq. (D-16d) Table 7
$c_{cr,Na} = \frac{s_{cr,Na}}{2} = \frac{11.7 \text{ in.}}{2} = 5.85 \text{ in.}$	-	Section 4.1.4 D.5.3.8 Eq. (D-16e)
$A_{Na} = (2 \cdot c_{cr,Na} + s) \cdot (c_{cr,Na} + c_{a,min})$ $= (2 \cdot 5.85 \text{ in.} + 4 \text{ in.}) \cdot (5.85 \text{ in.} + 2.5 \text{ in.}) = 131.1 \text{ in}^2$	-	Section 4.1.4 D.5.3.7
$A_{Nao} = (s_{cr,Na})^2 = (11.7 \text{ in.})^2 = 136.9 \text{ in}^2$	-	Section 4.1.4 D.5.3.7 Eq. (D-16c)

Calculation in accordance with ACI 318-05 Appendix D and th	is report	ACI 318 Code Ref.	Report Ref.
For $c_{a,min} < c_{cr.Na}$ $\psi_{ed,Na} = 0.7 + 0.3 \cdot \left(\frac{c_{a,min}}{c_{cr,Na}}\right) = 0.7 + 0.3 \cdot \left(\frac{2.5 \text{ in.}}{5.85 \text{ in.}}\right)$	= 0.828	-	Section 4.1.4 D.5.3.11 Eq. (D-16m)
$\tau_{k,\text{max,uncr}} = \frac{k_{c,\text{uncr}}}{\pi \cdot d} \cdot \sqrt{h_{\text{ef}} \cdot f'_{c}}$ $= \frac{24}{\pi \cdot 0.5 \text{in.}} \cdot \sqrt{9 \text{in.} \cdot 4,000 \text{psi}} = 2,899 \text{psi}$	-	Section 4.1.4 D.5.3.10 Eq. (D-16n) Table 6	
$\begin{aligned} \psi_{g,Nao} &= \sqrt{n} - \left[\left(\sqrt{n} - 1 \right) \cdot \left(\frac{\tau_{k,uncr}}{\tau_{k,max,uncr}} \right)^{1.5} \right] \\ &= \sqrt{2} - \left[\left(\sqrt{2} - 1 \right) \cdot \left(\frac{1,985 psi}{2,899 psi} \right)^{1.5} \right] = 1.18 \end{aligned}$		-	Section 4.1.4 D.5.3.10 Eq. (D-16h) Table 7
$\begin{aligned} \psi_{g,Na} &= \psi_{g,Nao} + \left[\left(\frac{s}{s_{cr,Na}} \right)^{0.5} \cdot \left(1 - \psi_{g,Nao} \right) \right] \\ &= 1.18 + \left[\left(\frac{4 \text{ in.}}{11.7 \text{ in.}} \right)^{0.5} \cdot \left(1 - 1.18 \right) \right] = 1.075 \end{aligned}$		-	Section 4.1.4 D.5.3.10 Eq. (D-16g)
$\psi_{ec,Na} = 1.0$ no eccentricity - loading is concentric		-	Section 4.1.4 D.5.3.11 Eq. (D-16j)
$\psi_{\text{p,Na}} = \frac{\text{max} c_{\text{a,min}}; c_{\text{cr,Na}} }{c_{\text{ac}}} = \frac{\text{max} 2.5 \text{ in.}; 5.85 \text{ in.} }{22.1 \text{in.}} = 0$	0.265	-	Section 4.1.4 D.5.3.14 Eq. (D-16p)
$N_{ao} = \tau_{k,uncr} \cdot \pi \cdot d \cdot h_{ef} = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in. \cdot 9 in. = 1,985 psi \cdot \pi \cdot 0.5 in.$	= 28,062 lb	-	Section 4.1.4 D.5.3.9 Eq. (D-16f)
$\begin{split} N_{ag} &= \frac{A_{Na}}{A_{Nao}} \cdot \psi_{ed,Na} \cdot \psi_{g,Na} \cdot \psi_{ec,Na} \cdot \psi_{p,Na} \cdot N_{ao} \\ N_{ag} &= \frac{131.1 in^2}{136.9 in^2} \cdot 0.828 \cdot 1.075 \cdot 1.0 \cdot 0.265 \cdot 28,06 \end{split}$	2lb = 6,339lb	-	Section 4.1.4 D.5.3.7 Eq. (D-16b)
$\phi_{d} = 0.65$		-	Table 7
$\phi \cdot N_{ag} = 0.65 \cdot 6,339 lb = 4,120 lb$		-	-
Step 5. Determine controlling strength:		D.4.1.2	-
Steel Strength in Tension $\phi \cdot N_{sa}$	= 26,610 lb		
Concrete Breakout Strength in Tension $\phi \cdot N_{cbg}$	= 8,372 lb		
Bond Strength in Tension $\phi \cdot N_{ag}$	= 4,120 lb	Controls = ϕN_n	0
Step 6. Convert strength to ASD using factor provided in Section $N_{\text{allow,ASD}} = \frac{\phi \cdot N_{\text{n}}}{\alpha} = \frac{4,120 \text{lb}}{1.48} = 2,784 \text{lb}$	ON 4.Z:	-	Section 4.2 Eq. (4-1)



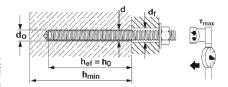
Hilti HIT-HY 150 MAX-SD

	HAS	Rebar	HI	-RB	HIT-	SZ (IP)	HIT	-DL
	NEW TOWNS WATER THE WATER							000
Ø[mm]	Ø[mm]	Ø[mm]	HIT-RB	Item no.	HIT-SZ	Item no.	HIT-DL	Item no.
12	10	8	12	336548	12	335022	12	371715
14	12	10	14	336549	14	335023	14	371716
16		12	16	336550	16	335024	16	371717
18	16	14	18	336551	18	335025	18	371718
20		16	20	336552	20	335026	20	371719
22		18	22	370774	22	380922	20	371719
24	20		24	380918	24	380923	20	371719
25		20	25	336553	25	335027	25	371720
28	24	22	28	380919	28	380924	25	371720
32		25	32	336554	32	335028	32	371721
	Ø[inch]	Size	HIT-RB	Item no.	HIT-IP	Item no.	HIT-DL	Item no.
7/16	3/8		7/16"	273203		-	-	-
1/2		#3	1/2"	273204	1/2"	274019	1/2"	38237
9/16	1/2	10M	9/16"	273205	9/16"	274020	9/16"	38238
5/8		#4	5/8"	273207	5/8"	274021	9/16"	38238
3/4	5/8	#5 & 15M	3/4"	273210	3/4"	274023	3/4"	38240
7/8	3/4	#6	7/8"	273211	7/8"	274024	7/8"	38241
1	7/8	#7 & 20M	1"	273212	1"	274025	1"	38242
1 1/8	1	#8	1 1/8"	273214	1 1/8"	274026	1"	38242
1 1/4		25M	1 1/4"	273216	1 1/4"	274027	1"	38242

Drill bits must conform to tolerances in ANSI B212-1994 Les mèches de forage doivent être conformes à ANSI B212-1994. Brocas deben cumplir con el estándar ANSI B212-1994.

Hilti HIT-HY 150 MAX-SD

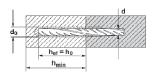
Setting Details of Hilti HIT-HY 150 MAX-SD with threaded rod



d	d ₀	h _{ef} min-max	T _{max} *	df	h _{min}	
[inch]	[inch]	[inch]	[ft-lb]	[inch]	[inch]	
3/8	7/16	2 3/8 - 7 1/2	15	7/16	h _{ef} + 1 1/4	
1/2	9/16	2 3/4 - 10	30	9/16	n _{Of} + 1 1/4	
5/8	3/4	3 1/8 - 12 1/2	60	11/16	h _{ef} + 2 d ₀	
3/4	7/8	3 1/2 - 15	100	13/16		
7/8	1	3 1/2 - 17 1/2	125	15/16	er . = -0	
1	1 1/8	4 - 20	150	1 1/8		
[mm]	[mm]	[mm]	[Nm]	[mm]	[mm]	
M10	12	60 - 200	20	12	h _{ef} + 30	
M12	14	70 - 240	40	14		
M16	18	80 - 320	80	18		
M20	24	90 - 400	150	22	h _{ef} + 2 d ₀	
M24	28	96 - 480	200	26		

"T _{max} : Edge Distance c _{ai} < (5 x d)					
Edge Distance cai	Anchor Spacing s _{min}	Maximum Torque			
1.75 in. (45 mm) ≤ cai < 5 x d	$5 \times d \le s_{min} < 16 \text{ in. } (406 \text{ mm})$	0.3 x T _{max}			
1.75 III. (45 IIIIII) ≤ Gai < 5 X G	s _{min} ≥ 16 in. (406 mm)	0.5 x T _{max}			

Setting Details of Hilti HIT-HY 150 MAX-SD with reinforcement bars



d	d ₀	h _{ef} min-max	h _{min}
US rebar	[inch]	[inch]	[inch]
# 3	1/2	2 3/8 - 7 1/2	hef + 1 1/4
# 4	5/8	23/4 - 10	
# 5	3/4	3 1/8 - 12 1/2	
# 6	7/8	3 1/2 - 15	$h_{ef} + 2 d_0$
#7	1	3 1/2 - 17 1/2	
#8	1 1/8	4 - 20	
Rebar [mm]	[mm]	[mm]	[mm]
10	14	60 - 200	h _{ef} + 30
12	16	70 - 240	
14	18	75 - 280	
16	20	80 - 320	$h_{ef} + 2 d_0$
20	25	90 - 400	
25	32	100 - 500	
CA rebar	[inch]	[inch]	[inch]
10 M	9/16	23/4 - 88/7	hef + 1 1/4
15 M	3/4	3 1/8 - 12 1/2	
20 M	1	3 1/2 - 15 3/8	$h_{ef} + 2 d_0$
25 M	1 1/4	4 - 19 7/8	

FIGURE 5—INSTRUCTIONS FOR USE (IFU) AS PROVIDED WITH PRODUCT PACKAGING (Continued)

HIIti HIT-HY 150 MAX-SD

Adhesive anchoring system for fastenings in concrete

Prior to use of product, follow instructions for use and recommended safety precautions. Check expiration date: See expiration date imprint on foilpack manifold. (Month/Year). Do not use an expired product.

Foil pack temperature: Must be between 32 °F and 104 °F (0 °C and 40 °C) when in use. Base material temperature at time of installation: Must be between 14 °F and 104 °F

Instructions for transport and storage: Keep in a cool, dry and dark place between 41 °F to 77 °F (5 °C to 25 °C)

Material Safety Data Sheet: Review the MSDS before use.

Installation instructions: Follow the illustrations on page 1 for the sequence of operations and refer to tables on page 2-3 for setting details. For any application not covered by this document, contact Hilti.

- $\label{eq:Drill hole} \begin{tabular}{ll} \textbf{Drill hole} to the required depth h_0 with a hammer drill set in rotation hammer mode using an appropriately sized carbide drill bit. For holes drilled with other drill types contact a Hilti representative. \\ \end{tabular}$
- 2 4 Clean hole: Cleaning method has to be decided based on borehole condition.

- Clean note: Cleaning method has to be decided based on borehole condition.
 Just before setting an anchor/rebar, the borehole must be free of dust, water and
 debris by one of the following methods:
 Method 1 for dry or water saturated concrete (refer to pictograms):
 Compressed air cleaning is permissible for all diameters and embedment depths.

 Blow from the back of the borehole with oil-free compressed air (min. 90ps) at 3.5
 CFM (6 bar at 6 m 3/h)) fully retracting the air extension 2 times until return air
 extension is free of extensible dust. stream is free of noticeable dust.
- Brush 2 times with the specified hillit HIT-RB brush size (brush $\emptyset \ge$ bore hole \emptyset) by inserting the round steel brush to the back of the borehole in a twisting motion and removing it. The brush should resist insertion into the borehole if not, the brush is too small and must be replaced with a brush of appropriate brush diameter.

 • Blow again with compressed air 2 times until return air stream is free of noticeable

If required use extensions for air nozzle and brushes to reach back of deep hole.

- Method 2 for standing water (e.g. water flows into cleaned borehole);
 Flush hole 2 times by inserting a water hose (water-line pressure) to the back of the borehole until water runs clear.
 Brush 2 times with the specified Hilti HIT-RD brush size (brush Ø ≥ borehole Ø) by
- inserting the round steel brush to the back of the borehole with a twisting motion and removing it. The brush should resist insertion into the borehole - if not, the brush is too small and must be replaced with a brush of appropriate brush diameter.

 • Flush again 2 times until water runs clear. Remove all standing water completely (i.e.
- vacuum, compressed air or other appropriate procedure). To attain a dried borehole, a Hilli HIT-DL air nozzle attachment is recommended for borehole depth \leq 10 inch (250 mm) and required for borehole depth > 10 inch (250 mm).
- Insert foil pack in foil pack holder. Never use damaged foil packs and/or damaged or unclean foil pack holders. Attach new mixer prior to dispensing a new foil pack (snug fit). 5
- Tightly attach Hilti HIT-RE-M mixer to foil pack manifold. Do not modify the mixer in any way. Make sure the mixing element is in the mixer. Use only the mixer supplied 6 with the anchor adhesive.
- **Insert foil pack holder with foil pack into HIT-dispenser.** Push release trigger, retract plunger and insert foil pack holder into the appropriate Hilti dispenser. 7
- Discard initial anchor adhesive. The foil pack opens automatically as dispensing is initiated. Do not pierce the foilpack manually (can cause system failure). Depending on the size of the foil pack an initial amount of anchor adhesive has to be discarded. See pictogram 8 for discard quantities. Dispose discarded anchor adhesive into the empty outer packaging, if a new mixer is installed onto a previously-opened foil pack, the first trigger pulls must also be discarded as described above. For each new foil pack a new mixer must be used. 8
- 9 11 Inject anchor adhesive from the back of the borehole without forming air voids:
- Inject anchor adhesive from the back of the borehole without forming air voids:

 Injection method for borehole with depth ≤10 inch/250 mm:
 Inject the anchor adhesive starting at the back of the hole (use the extension for deep holes), slowly withdraw the mixer with each trigger pull. Fill holes approximately 2/3 full, or as required to ensure that the annular gap between the anchor/rebar and the concrete is completely filled with anchor adhesive along the embedment length. After injection is completed, depressurize the dispenser by pressing the release trigger. This will prevent further anchor adhesive discharge from the mixer.

 Piston plug injection is recommended for borehole depth > 10 inch/250 mm.

 The installation overhead is only possible with the aid of piston plugs.

 Assemble HIT-RE-M mixer, extension(s) and appropriately sized piston plug, lnsert piston plug HIT-SZI/P to back of the hole, and inject anchor adhesive as described in the injection method above. During injection the piston plug will be naturally extruded out of the bore hole by the anchor adhesive pressure.
- lisert anchor/rebar into bore hole. Mark and set anchor/rebar to the required embedment depth. Before use, verify that the anchor/rebar is dry and free of oil and other contaminants. To ease installation, anchor/rebar may be slowly twisted as they are inserted. Use only Hillt anchor rods or equivalent. After installing an anchor/rebar, the annular gap must be completely filled with anchor adhesive.

 Attention! For overhead applications take special care when inserting the anchor/rebar. Excess adhesive will be forced out of the borehole take appropriate steps to prevent it from falling onto the installer. Position the anchor/rebar and secure it from proving/falling during the curing time (e.g. wedges). 12

moving/falling during the curing time (e.g. wedges).

- Observe the get lime "t_{get}", which varies according to temperature of base material. Minor adjustments to the anchor/rebar position may be performed during the get time. See table 12. Once the get time has elapsed, do not disturb the anchor/rebar until the curing time "t_{cure}" has elapsed. 13
- Apply designed load/torque after" t cure" has passed, and the fixture to be attached 14 has been positioned. See table 13.

Partly used foil packs must be used up within four weeks. Leave the mixer attached on the foil pack manifold and store under the recommended storage conditions. If reused, attach a new mixer and discard the initial quantity of anchor adhesive as described by point 8.

HIIti HIT-HY 150 MAX-SD

Safety instructions:

For industrial use only. Keep out of the reach of children. See the Material Safety Data Sheet for this product before handling.

Caution: Irritating to eyes and skin. May cause sensitization in susceptible individuals

Contains: dibenzoyl peroxide.

Precautions: Avoid contact with skin/eves. Always wear impermeable gloves and eye protection when using product. Store in a cool, dry area. Keep from freezing. Do not store in direct sunlight.

First Aid: Eyes - Immediately flush with water for 15 minutes

contact a physician. **Skin** - Wash with soap and water launder contaminated clothing before reuse. If irritations occurs, contact physician.

Ingestion - Do not induce vomiting unless directed by a physician. Contact a physician immediately Inhalation - Move to fresh air, give oxygen if breathing is difficult. contact a physician if symptoms persist.



In Case of Emergency, call Chem-Trec: En cas d'urgence, téléphoner Chem-Trec: En Caso de Emergencia, llame Chem-Trec: 1-800-424-9300 (USA, P.R., Virgin Islands, Canada) 1-800-424-9300 (USA, P.R., Virgin Islands, Canada) 001-703-527-3887 (other countries/autres pays/otros países)

Made in Germany

Net contents: 11.1 fl. oz (330 ml)/16.9 fl. oz (500 ml)

Net weight: 20.3 oz (575 g)/31.0 oz (880 g)

Warranty: Refer to standard Hilti terms and conditions of sale for warranty information

Failure to observe these installation instructions, use of non-Hilti anchors, poor or questionable concrete conditions, or unique applications may affect the reliability or performance of the fastenings.



ICC-ES Evaluation Report

ESR-3013 Supplement

Reissued April 1, 2011

This report is subject to renewal in two years.

www.icc-es.org | (800) 423-6587 | (562) 699-0543

A Subsidiary of the International Code Council®

DIVISION: 03 00 00—CONCRETE Section: 03 16 00—Concrete Anchors

REPORT HOLDER:

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www.us.hilti.com
HiltiTechEng@us.hilti.com

EVALUATION SUBJECT

HILTI HIT-HY 150 MAX-SD ADHESIVE ANCHORING SYSTEM FOR CRACKED AND UNCRACKED CONCRETE

1.0 EVALUATION SCOPE

Compliance with the following codes:

- 2007 Florida Building Code—Building
- 2007 Florida Building Code—Residential

Property evaluated:

Structural

2.0 PURPOSE OF THIS SUPPLEMENT

This supplement is issued to indicate that the Hilti HIT-HY 150 MAX-SD Adhesive Anchoring System for cracked and uncracked concrete, as described in the master report, complies with the 2007 Florida Building Code—Building, and the 2007 Florida Building Code—Residential, when designed and installed in accordance with the master evaluation report.

Use of the Hilti HIT-HY 150 MAX-SD Adhesive Anchoring System for cracked and uncracked concrete, as described in the master evaluation report, to comply with the High Velocity Hurricane Zone Provisions of the 2007 *Florida Building Code—Building* has not been evaluated, and is outside the scope of this supplement.

For products falling under Florida Rule 9N-3, verification that the report holder's quality assurance program is audited by a quality assurance entity approved by the Florida Building Commission for the type of inspections being conducted is the responsibility of an approved validation entity (or the code official when the report holder does not possess an approval by the Commission).

This supplement expires concurrently with the master evaluation report issued on April 1, 2011.



MSDS No.: 330 **Revision No.:** 001 Revision Date: 04/28/10 Page: 1 of 2

MATERIAL SAFETY DATA SHEET

HIT- HY150 MAX SD Product name:

Description: Methacrylate resin and hardener. Part A is in the large tube; Part B is in the small tube.

Supplier: Hilti, Inc. P.O. Box 21148, Tulsa, OK 74121

Emergency # (Chem-Trec.): 1 800 424 9300 (USA, PR, Virgin Islands, Canada); 001 703 527 3887 (other countries)

INGREDIENTS AND EXPOSURE LIMITS

Ingredients:		CAS Number:	TLV:	PEL:	STEL:
Part A:	Quartz sand	14808-60-7	0.05 mg/m ³ (R)	0.1 mg/m ³ (R)	NE
	1,4 Butanediol Dimethacrylate	2082-81-7	NE	NE 3	NE
Part B:	Quartz sand	14808-60-7	0.05 mg/m ³ (R)	<u>10 mg/m³</u> (R) %SiO₂ + 2	NE
	Aluminum oxide	001344-28-1	10 mg/m ³	5 mg/m ³ (R)	NE
	Dibenzoyl peroxide	00094-36-0	5 mg/m ³	5 mg/m ³	NE
	Amorphous silica	07631-86-9	10 mg/m ³	20 mppcf	NE

Abbreviations: NJ TSRN indicates New Jersey Trade Secret Registry Number. (R) indicates "as respirable dust". (N) indicates "as nuisance dust". PEL = OSHA Permissible Exposure Limit. TLV = ACGIH Threshold Limit Value. STEL = Short Term Exposure Limit (15 minute time-weighted average). NE = None Established. mppcf = million particles per cubic foot. (M) = Mist

PHYSICAL DATA

Appearance and Odor: Gray paste. Ester-like odor. **VOC Content:** 7.0 g/l **Boiling Point:** Not determined Vapor Pressure (@68 º F) 0 mm Hg Not determined Not determined Vapor Density: (air = 1) **Odor Threshold Solubility in Water:** Insoluble **Evaporation Rate:** Not determined **Specific Gravity:** 6-7 1.8

FIRE AND EXPLOSION HAZARD DATA

Flash Point: 228° F Flammable Limits: Not determined

Extinguishing Media: CO₂, Dry Chemical, Foam, Water spray

Special Fire Fighting

Procedures:

Unusual Fire and Explosion

Hazards:

Use a self-contained breathing apparatus when fighting fires involving chemicals.

None known. Thermal decomposition products can be formed.

REACTIVITY DATA

Stability: Dibenzoyl peroxide decomposes (non-violently) at 150° F. Ignition does not occur due to the

water content (> 5%).

Hazardous Polymerization: Will not occur.

Incompatibility: Strong acids and oxidizing agents. Do not store in direct sunlight.

Decomposition Products: Thermal decomposition can yield CO, CO₂ and NO_x.

Avoid temperature extremes which could shorten the shelf-life of this product: i.e. below 41° F Conditions to Avoid:

freezing and above 77° F. (See handling and storage requirements).

HEALTH HAZARD DATA

Known Hazards:

Eye and skin irritation. Possible sensitizer.

Signs and Symptoms of

Exposure:

Eyes: can cause irritation. **Skin:** Prolonged and repeated contact can cause irritation. An allergic skin reaction (sensitization e.g. rash, itching, reddening) can occur with some individuals. **Inhalation:** Possible irritation. **Ingestion:** Not a likely route of exposure.

Contact. Inhalation.

Routes of Exposure: Carcinogenicity:

IARC classifies crystalline silica (quartz sand) as a Gp I carcinogen based upon evidence among workers in industries where there has been long-term and chronic exposure (via inhalation) to silica dust; e.g. mining, quarry, stone crushing, refractory brick and pottery workers. This product

does not pose a dust hazard; therefore, this classification is not relevant.

Medical Conditions Aggravated by Exposure: Eye, skin, and respiratory conditions.

EMERGENCY AND FIRST AID PROCEDURES

Eyes: Flush with plenty of water. Contact a physician if symptoms occur.

Skin: Wash with soap and water.

Inhalation: Move victim to fresh air. Call a physician if symptoms persist.

Ingestion: Contact a physician immediately. Do not induce vomiting unless directed by a physician.

Other: Referral to a physician is recommended if there is any question about the seriousness of the

injury/exposure.

CONTROL MEASURES AND PERSONAL PROTECTIVE EQUIPMENT

Ventilation: General (natural or mechanically induced fresh air movements).

Eve Protection: Safety glasses.

Impermeable gloves recommended. **Skin Protection:**

Respiratory Protection: None normally required. Where ventilation is inadequate to control vapors, use a NIOSH-

approved respirator with organic vapor cartridges. Never enter a confined space without an appropriate air supplied respirator. If dusts are generated during demolition or removal, wear an

appropriate dust mask or respirator.

PRECAUTIONS FOR SAFE HANDLING AND USE

Handling and Storing

Precautions:

Store in a cool, dry area preferably between 41° and 77° F. Do not store in direct sunlight. Keep away from open flames, heat sources and sparks. Avoid prolonged or repeated contact. Use with adequate ventilation. Always wash thoroughly after handling chemical products. For

industrial use only. Keep out of reach of children.

Take up with an absorbent material and place in a container for proper disposal. **Spill Procedures:**

REGULATORY INFORMATION

This MSDS has been prepared in accordance with the federal OSHA Hazard Communication **Hazard Communication:**

Standard. 29 CFR 1910.1200.

HMIS Codes: Health 1, Flammability 1, Reactivity 0, PPE B

DOT Shipping Name: Not regulated IATA / ICAO Shipping Name: Not regulated

All other chemical components listed on TSCA inventory. **TSCA Inventory Status:**

This product contains 5 - 10% Benzoyl peroxide (CAS #94-36-0) which is subject to reporting under Section 313 of SARA Title III (40 CFR Part 372). **SARA Title III, Section 313:**

EPA Waste Code(s): Not regulated by EPA as a hazardous waste

Waste Disposal Methods: Consult with regulatory agencies or your corporate personnel for disposal methods that comply

with local, state, and federal safety, health and environmental regulations.

CONTACTS

Customer Service: 1 800 879 8000 **Technical Service:** 1 800 879 8000

Health / Safety: 1 800 879 6000 (x1003704) Jerry Metcalf

Emergency # (Chem-Trec): 1 800 424 9300 (USA, PR, Virgin Islands, Canada); 001 703 527 3887 (other countries)

The information and recommendations contained herein are based upon data believed to be correct; however, no guarantee or warranty of any kind expressed or implied is made with respect to the information provided.